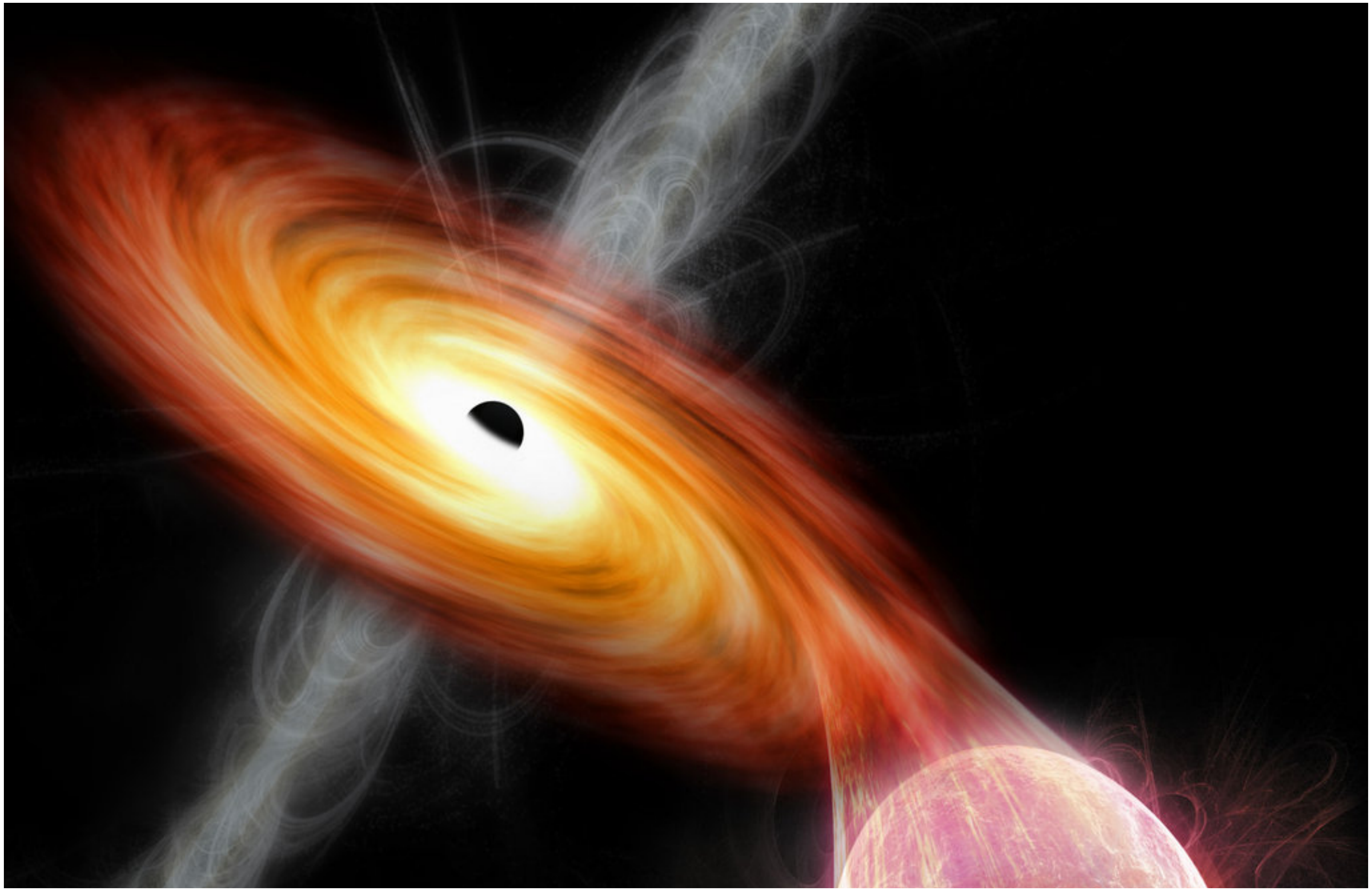
High Energy Astrophysics

Dr. Adam Ingram



Schedule

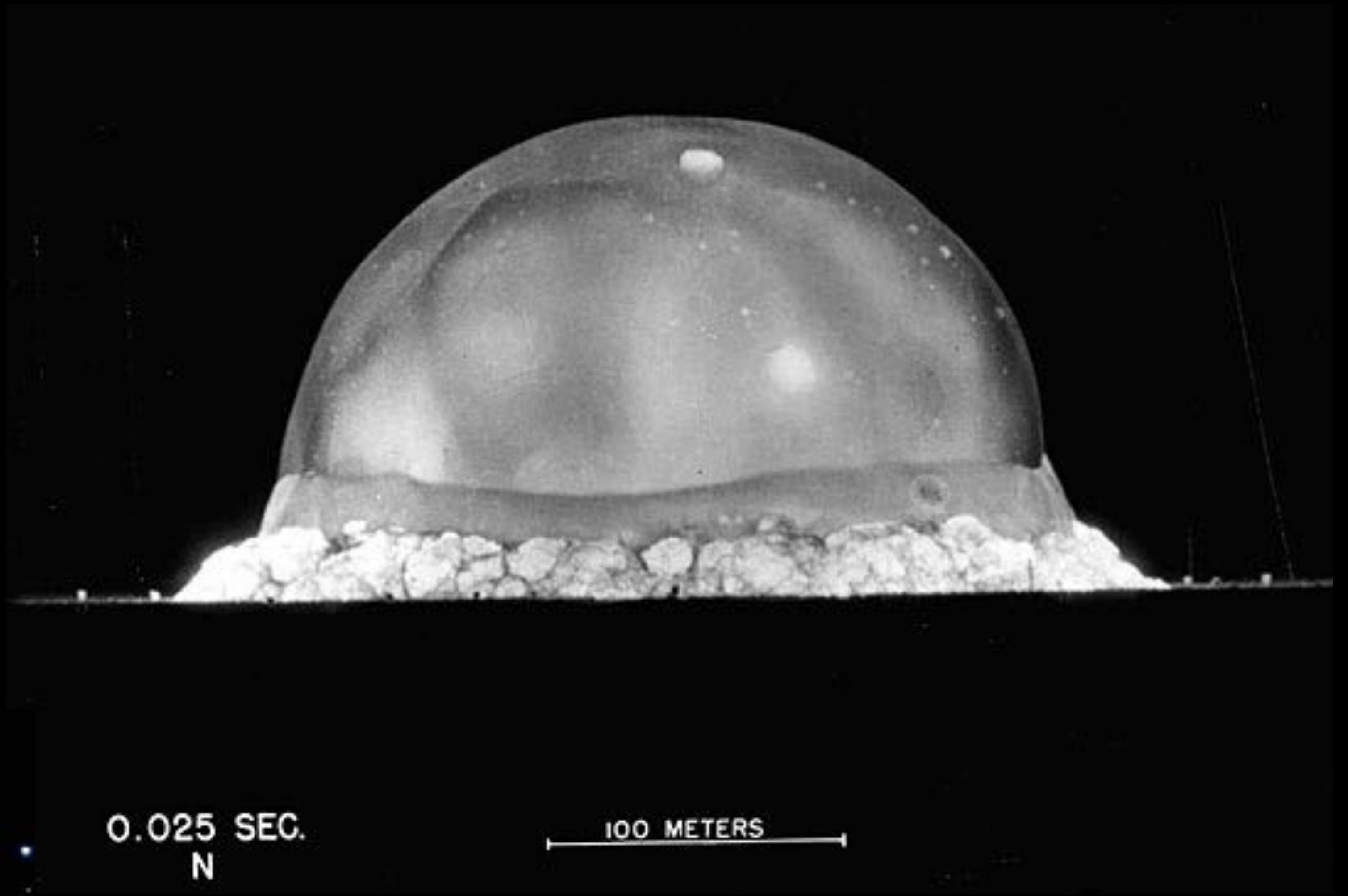
- ***Lecture 1: Shocks*** — Blast waves from huge explosions, strong shock conditions at the front of the blast wave.
- ***Lecture 2: Shock Acceleration*** — How electrons are accelerated to ultra-relativistic energies at strong shock fronts.
- ***Lecture 3: Synchrotron Radiation*** — The emission mechanism.
- ***Lecture 4: Synchrotron Radiation*** — Synchrotron self-absorption and spectral ageing.
- ***Lecture 5: Accretion discs*** — Structure, luminosity and spectrum.
- ***Lecture 6: The X-ray Corona*** — Thermal Compton scattering, X-ray reflection.
- ***Lecture 7: Black holes and Jets*** — The AGN zoo, evidence for black holes, jet mechanisms, super-luminal jet motion.
- ***Lecture 8: Galaxy Clusters*** — Thermal bremsstrahlung radiation, Sunyaev-Zeldovich effect.

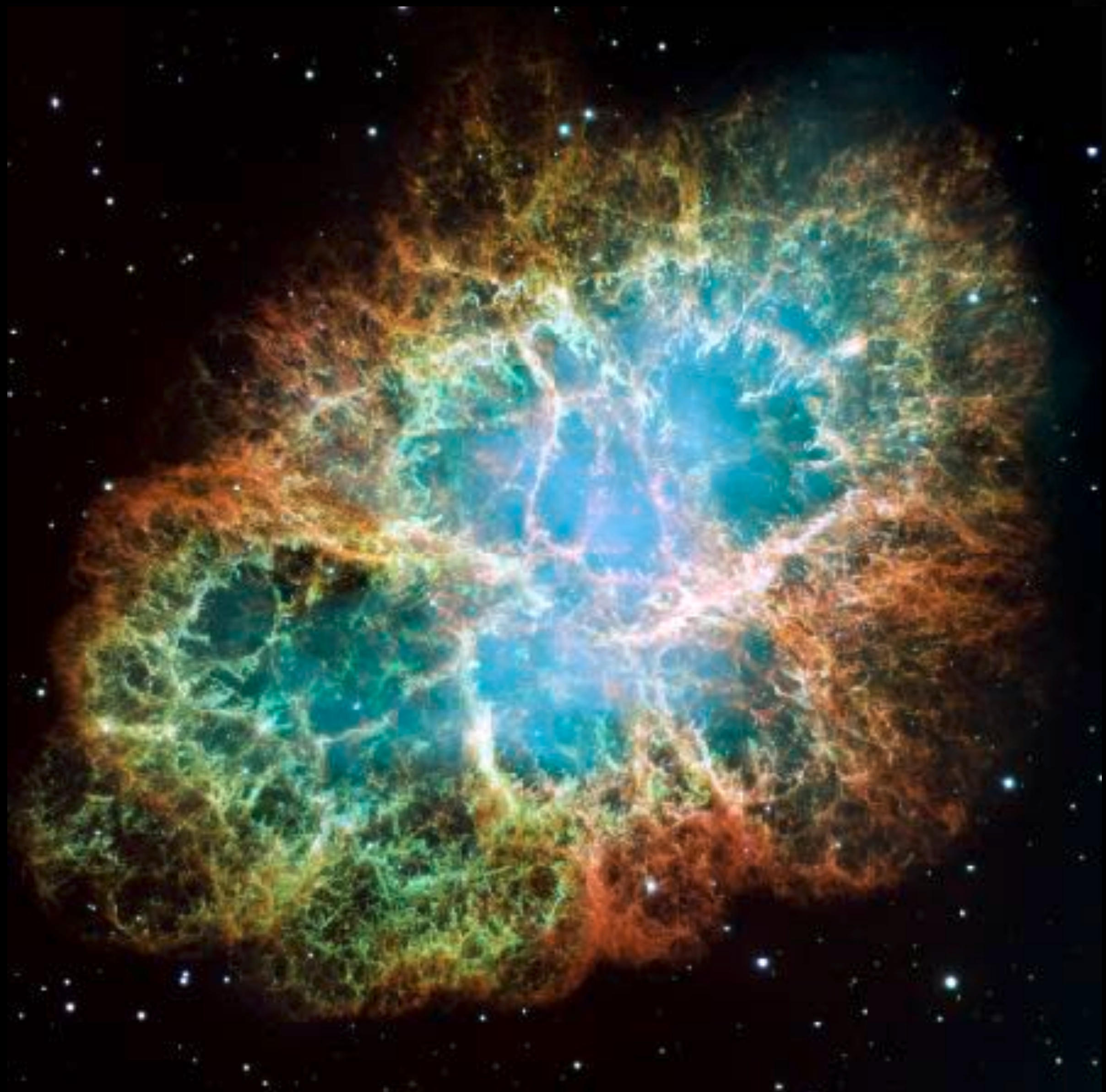
Reading Material

- “High Energy Astrophysics” by Malcolm Longair
- “Accretion Power in Astrophysics” by Frank, King & Raine
- “Radiative Processes in Astrophysics” by Rybicki & Lightman

Questions: Online question session, can also email me!

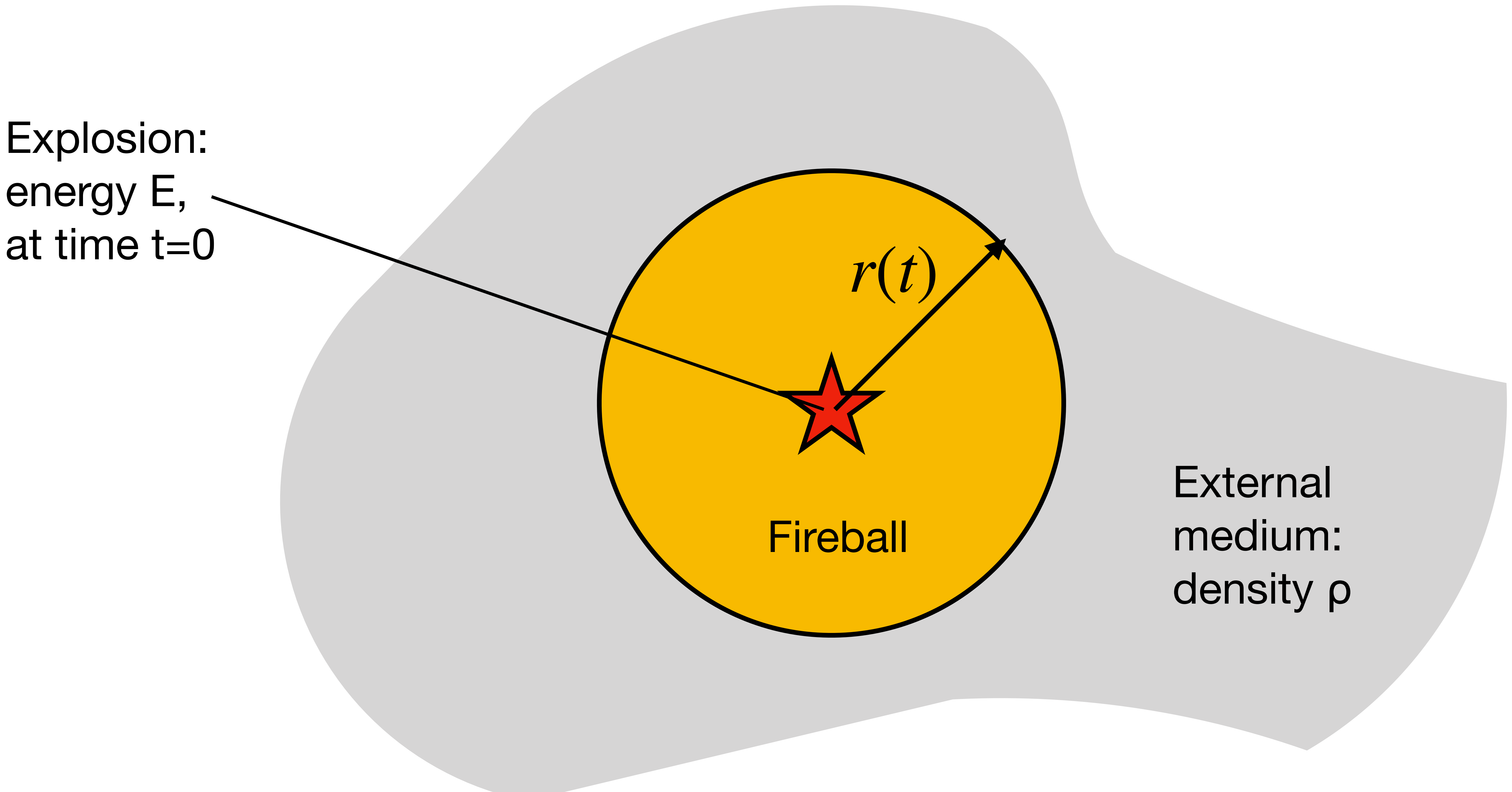
Lecture 1
Shocks





Blast waves

After an explosion (e.g. supernova, atomic bomb) a fireball expands outwards



Blast waves

- In 1950, G. I. Taylor calculated how the fireball expansion relates to explosion energy and external density
- He reduced the problem to a self-similar scaling solution — basically using dimensional analysis.
- He reasoned that r is a function of E, ρ and t:

Blast waves

- In 1950, G. I. Taylor calculated how the fireball expansion relates to explosion energy and external density
- He reduced the problem to a self-similar scaling solution — basically using dimensional analysis.
- He reasoned that r is a function of E, ρ and t:

$$r = C\underbrace{\rho^{x}E^{y}t^{z}}_{\text{Must have dimensions of length}}$$

Dimensionless constant

Blast waves

$$r = C\rho^x E^y t^z$$

Blast waves

$$r = C\rho^x E^y t^z$$

$$\Longrightarrow$$

$$m = [\mathrm{kg\ m^{-3}}]^x\ [\mathrm{kg\ m^2\ s^{-2}}]^y\ [s]^z$$

$$m = \mathrm{kg}^{x+y}\ \mathrm{m}^{-3x+2y}\ \mathrm{s}^{-2y+z}$$

Blast waves

$$r = C\rho^x E^y t^z$$

$$\Longrightarrow$$

$$m = [\mathrm{kg\ m}^{-3}]^x\ [\mathrm{kg\ m}^2\ \mathrm{s}^{-2}]^y\ [s]^z$$

$$m = \mathrm{kg}^{x+y}\ \mathrm{m}^{-3x+2y}\ \mathrm{s}^{-2y+z}$$

$$\Longrightarrow$$

$$0 = x + y$$ …mass

$$1 = -3x + 2y$$ …length

$$0 = -2y + z$$ …time

Blast waves

$$r = C\rho^x E^y t^z$$

$$\Longrightarrow$$

$$0 = x + y$$

$$1 = -3x + 2y$$

$$0 = -2y + z$$

$$\Longrightarrow$$

$$x = -1/5$$

$$y = 1/5$$

$$z = 2/5$$

Blast waves

$$r = C\rho^x E^y t^z$$

$$\Longrightarrow$$

$$0 = x + y$$
$$1 = -3x + 2y$$
$$0 = -2y + z$$

$$\Longrightarrow$$

$$x = -1/5 \quad \therefore \quad r = C\rho^{-1/5}E^{1/5}t^{2/5}$$
$$y = 1/5$$
$$z = 2/5$$

Blast waves

$$r = C\rho^{-1/5}E^{1/5}t^{2/5}$$

$$\Longrightarrow$$

$$E = D\frac{r^5\rho}{t^2}$$

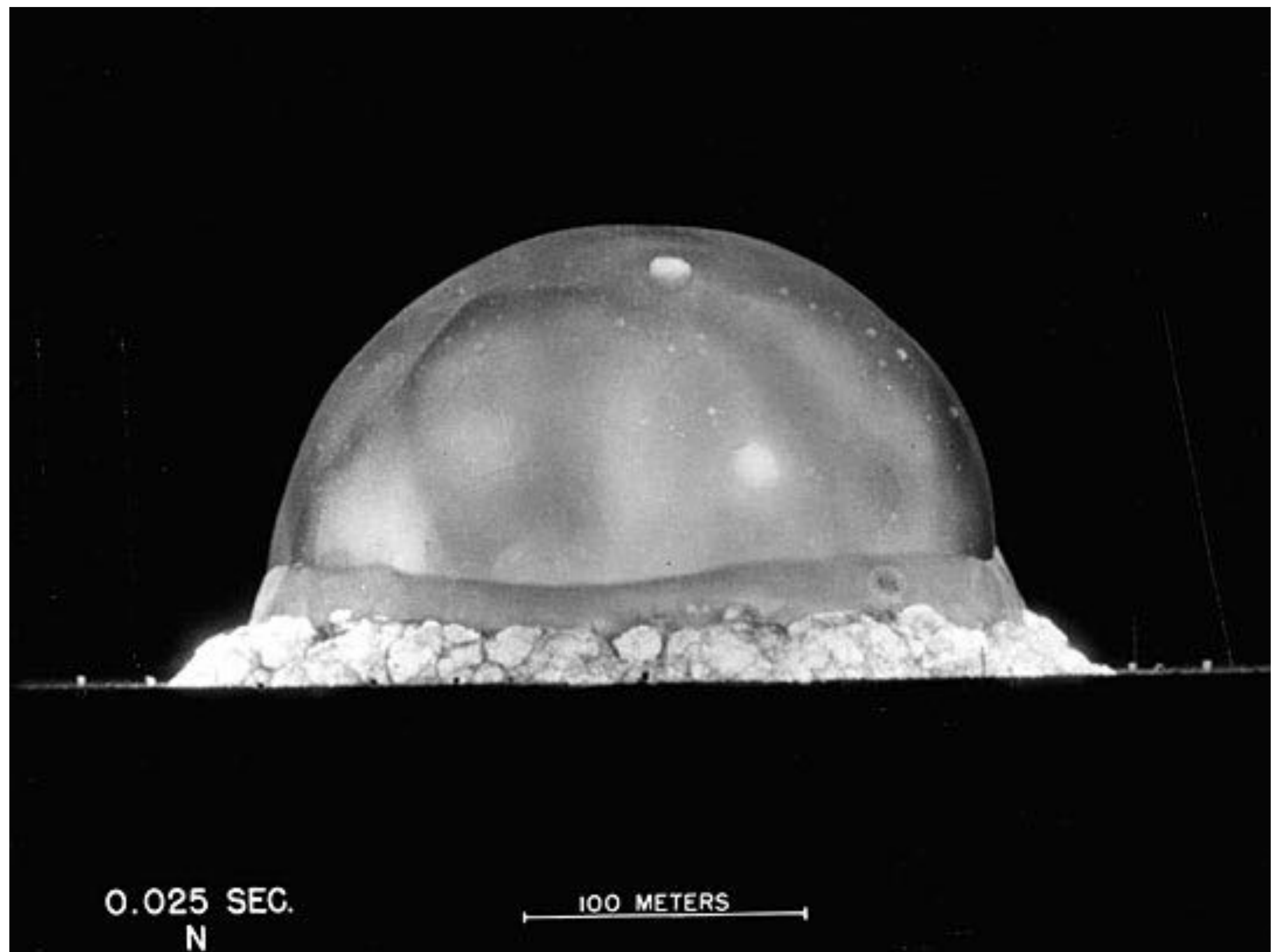
- Taylor used high-speed photographs of small detonations in the lab to determine that D~1.033 for a fireball expanding into air.
- The power of dimensional analysis is that even though the experiments were done on very small scales, we can be sure the scaling will still hold for explosions that are many, many orders of magnitude greater.
- Sedov later came up with a full solution (see: http://www.mso.anu.edu.au/~geoff/AGD/Sedov.pdf), and so the above formula is usually referred to as the *Taylor-Sedov solution*.

Blast waves

- Taylor used his equation and de-classified photos of the 1st atomic bomb tests to calculate the yield of the bomb.

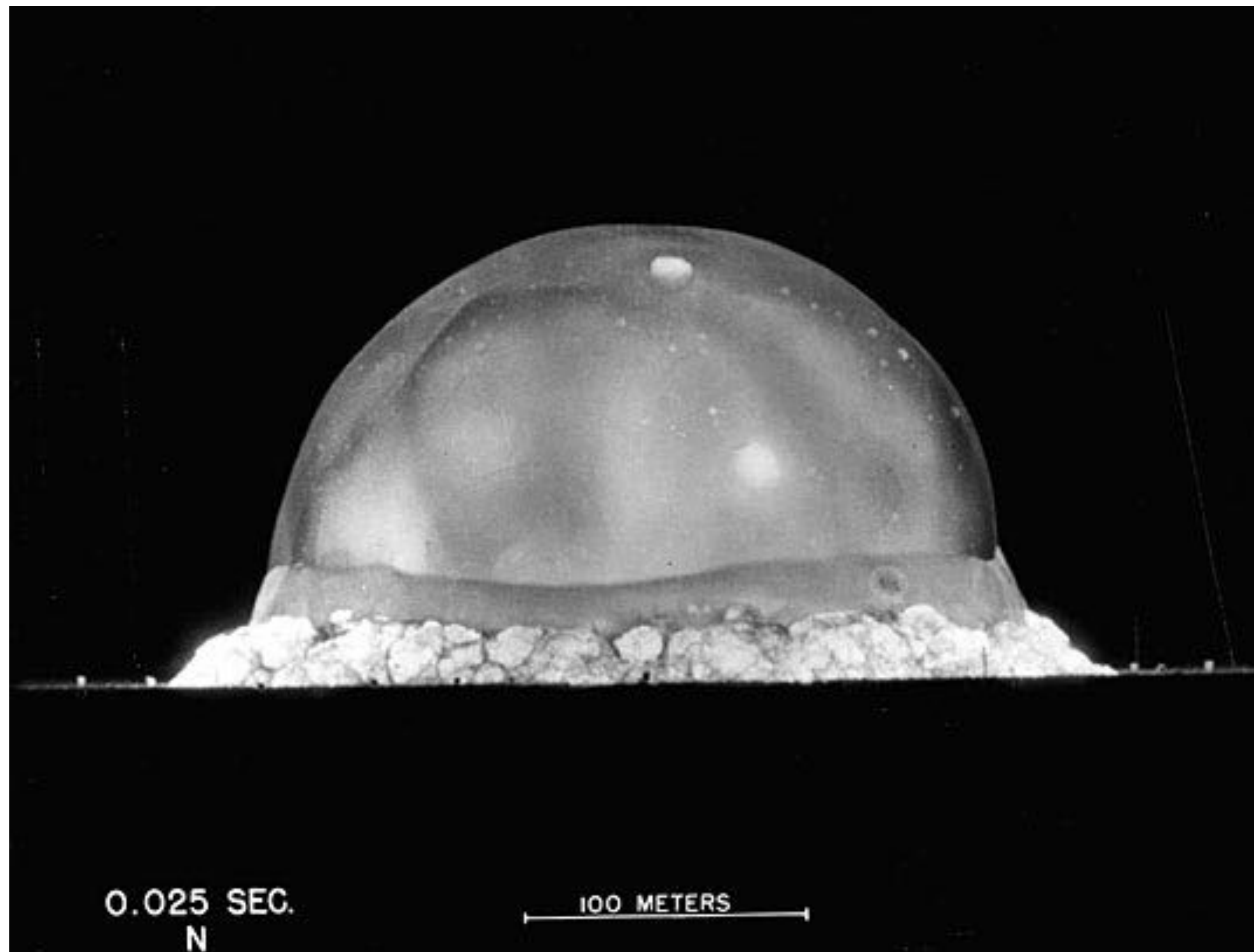
$$E \approx 1.033 \frac{r^5 \rho}{t^2}$$

$$\rho \approx 1.1 \text{ kg m}^{-3}$$
$$r \approx 140 \text{ m}$$
$$t = 25 \text{ ms}$$
$$\Longrightarrow$$
$$E \approx 9.778 \times 10^{13} \text{ J}$$
$$E \approx 23.28 \text{ kilotons}$$



Blast waves

- Taylor used his equation and de-classified photos of the 1st atomic bomb tests to calculate the yield of the bomb.
- The true (still classified in 1950) yield of the bomb was ~18-20 kilotons!!



$$E \approx 23.28 \text{ kilotons}$$

Blast waves

- Now calculate fluency of the Crab supernova of 1054

$$E \approx \frac{r^5 \rho}{t^2}$$

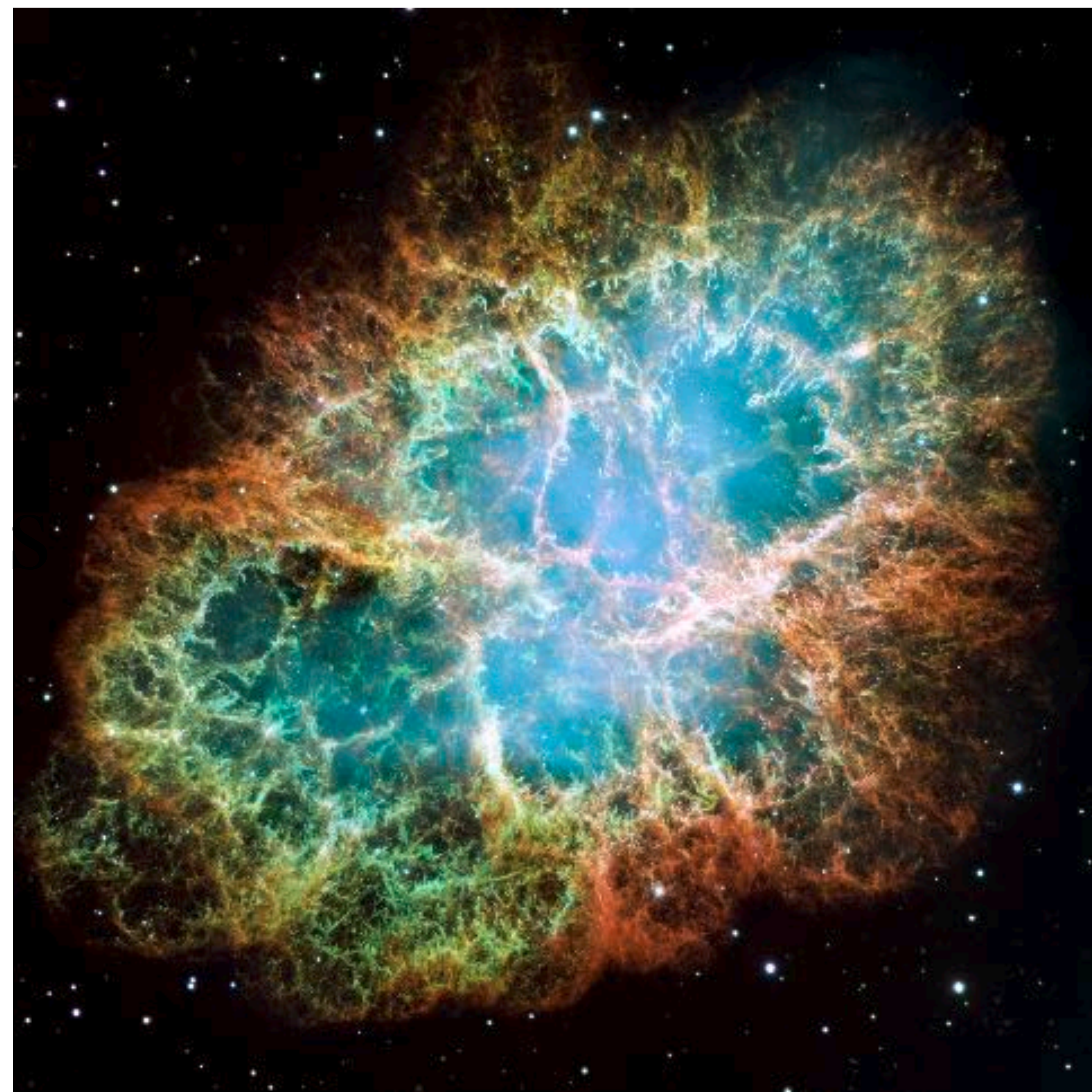
$$\rho \approx 10^{-21} \text{ kg m}^{-3}$$

$$r \approx 3 \text{ pc} \sim \ 9 \times 10^{16} \text{ m}$$

$$t = 966 \text{ yrs} \sim 3 \times 10^{10}$$

$$\Longrightarrow$$

$$E \approx 6.6 \times 10^{42} \text{ J}$$

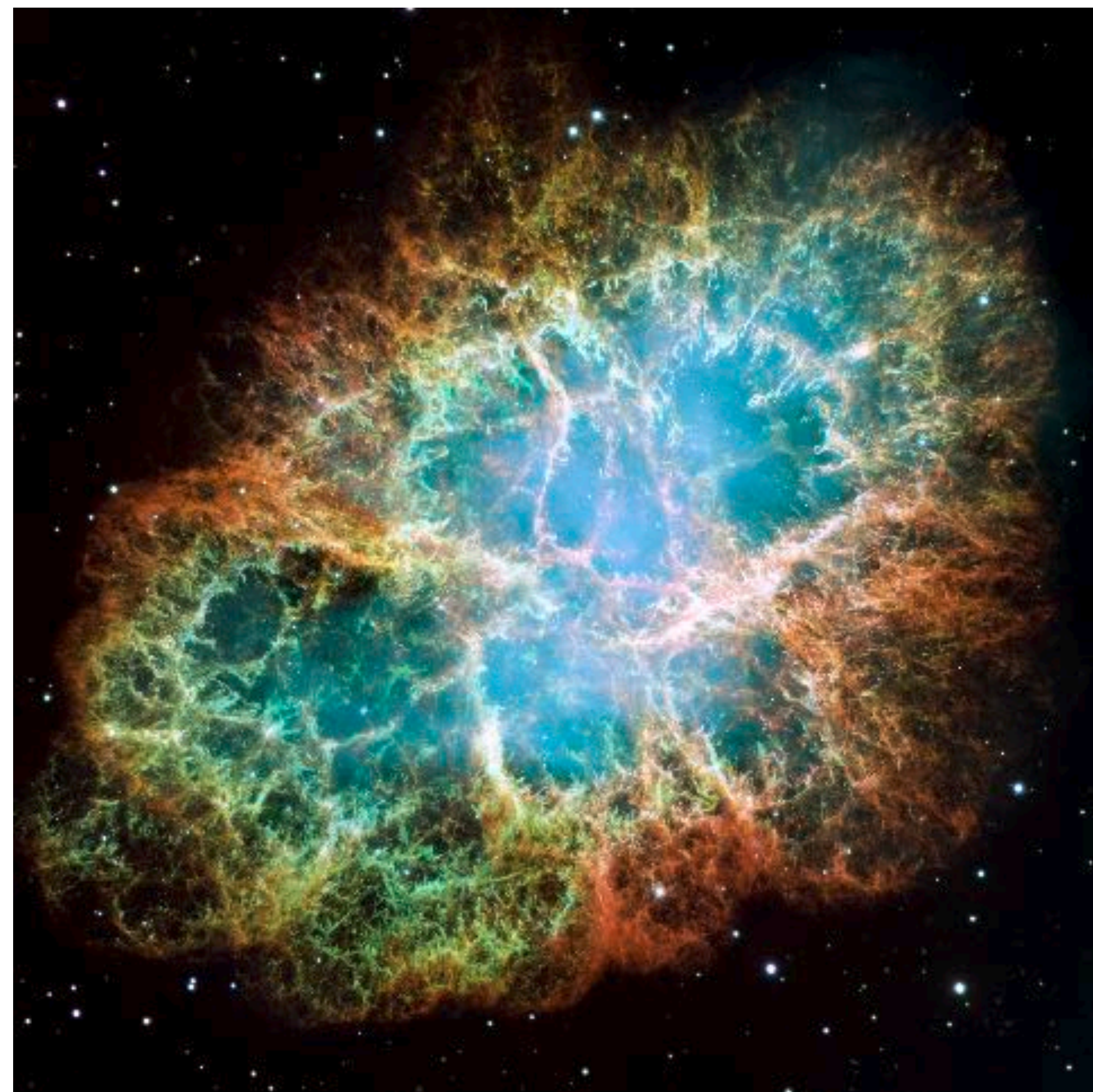


Blast waves

- What about the current speed of the blast wave?

$$\dot{r} \approx (2/5)\rho^{-1/5}E^{1/5}t^{-3/5}$$

$$\dot{r} \approx 1.2 \times 10^6 \text{ m/s}$$



Blast waves

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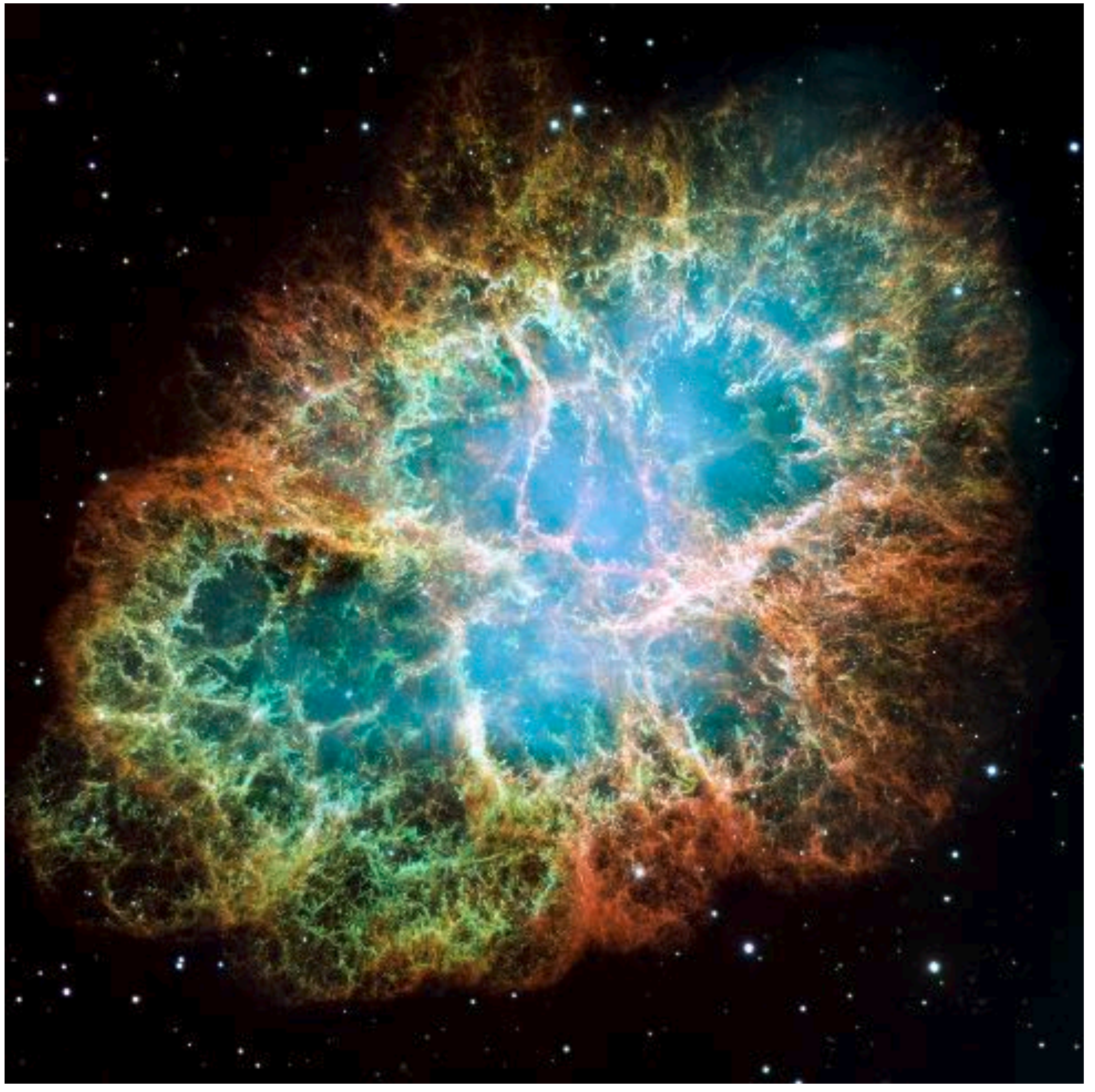
$$\dot{r} \approx (2/5)\rho^{-1/5}E^{1/5}t^{-3/5}$$

$$\dot{r} \approx 1.2 \times 10^6 \text{ m/s}$$

$$\dot{r} \gg c_s$$

$$\therefore$$

Blast wave is supersonic!



Blast waves

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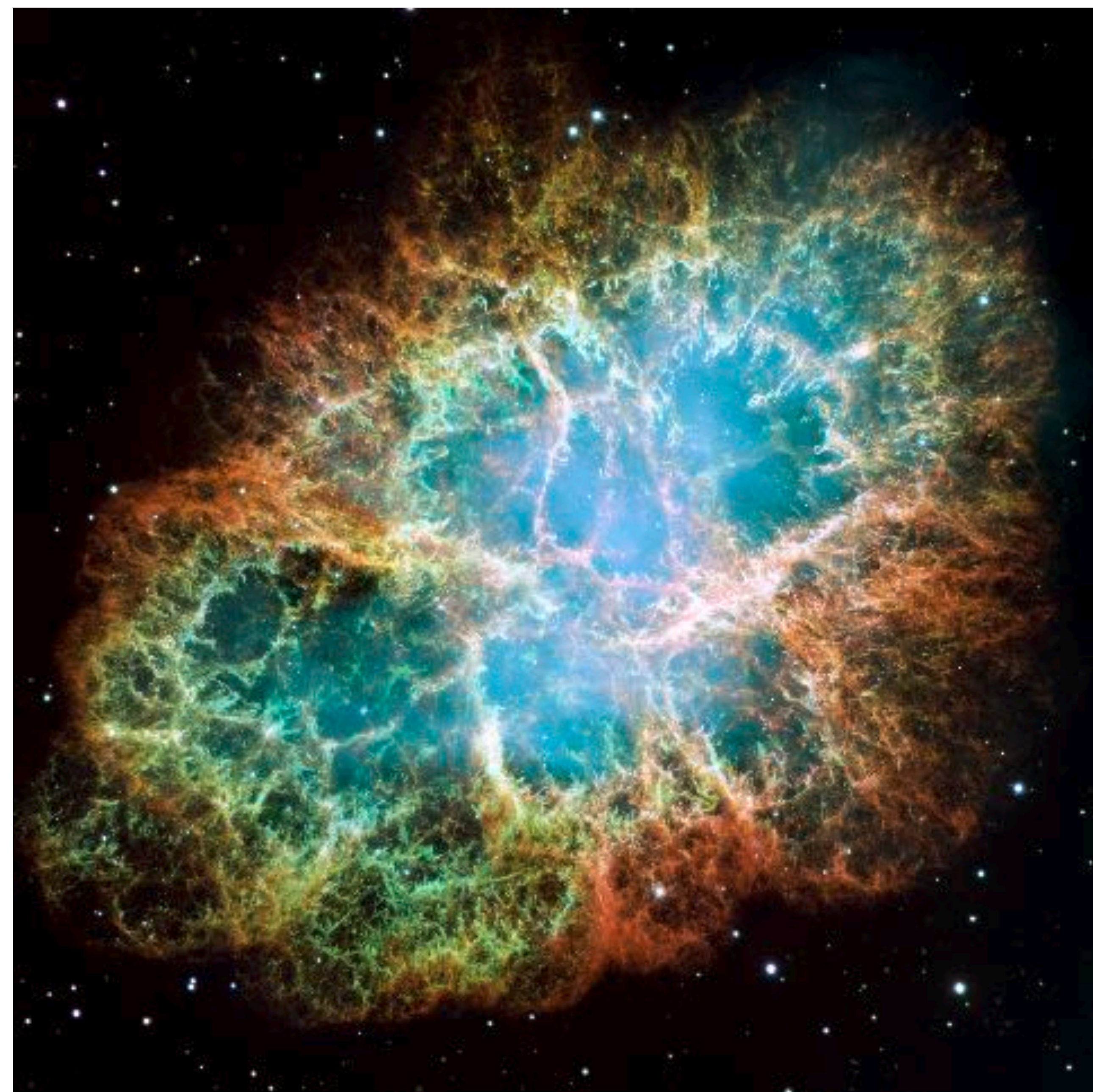
$$\therefore$$

Blast wave is supersonic!

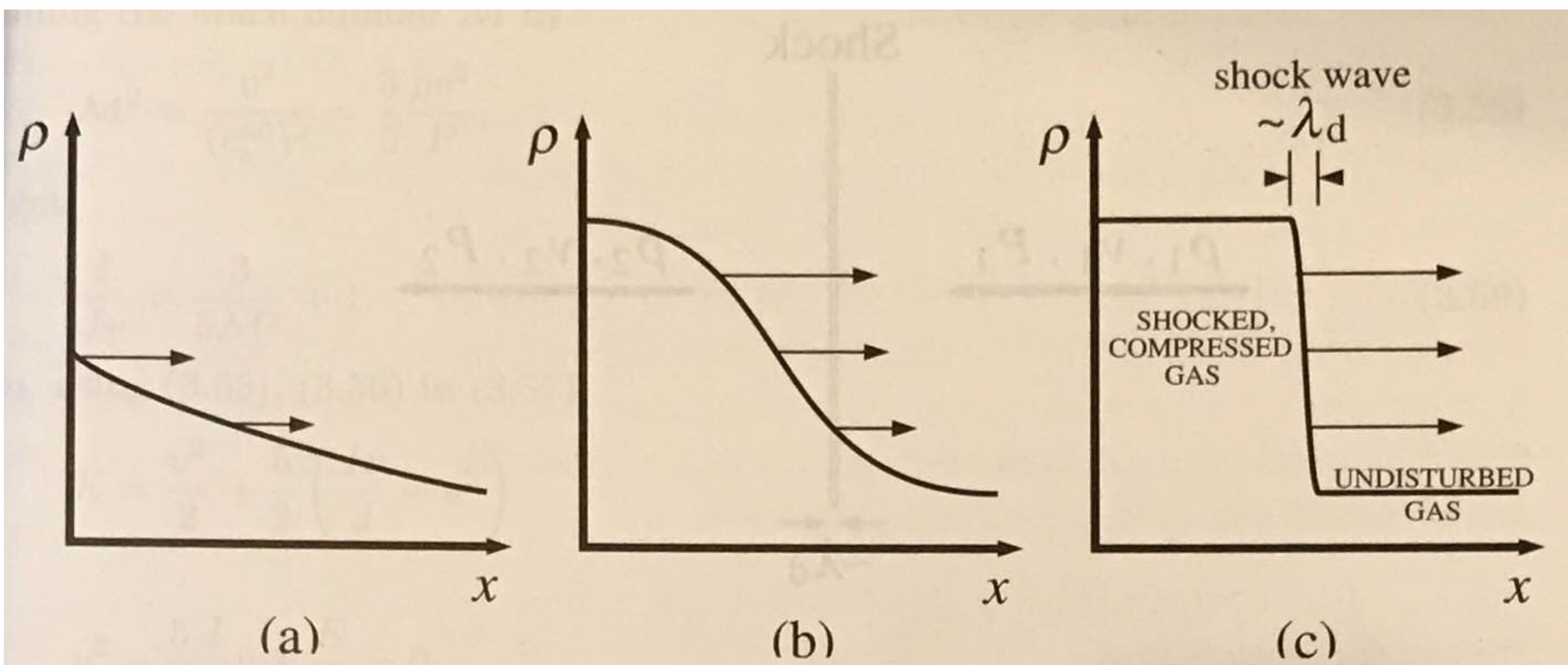
$$\therefore$$

Shock!



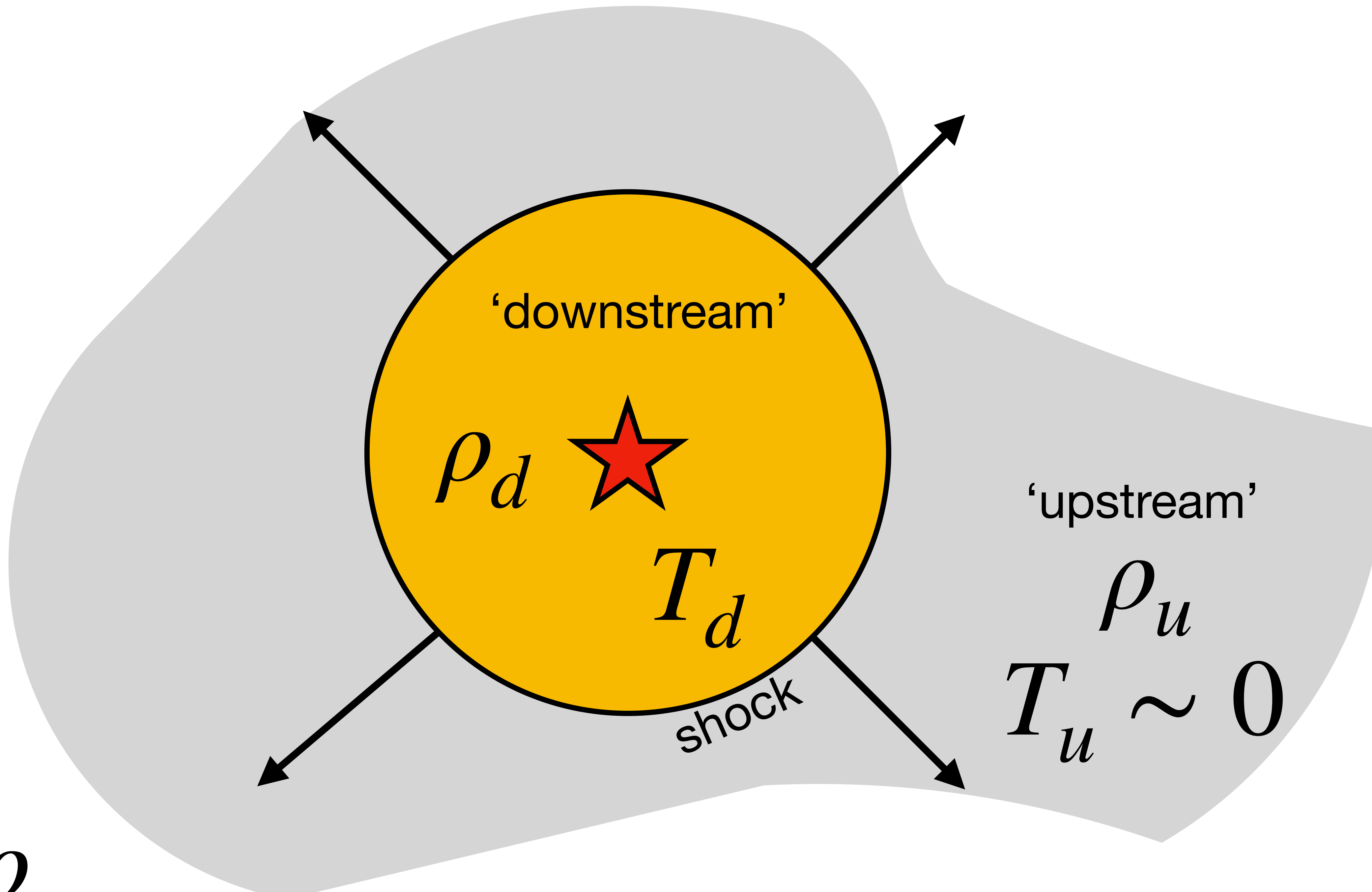
Shocks

- A shock occurs when a disturbance moves through a medium faster than the sound speed in the medium, i.e., sufficiently fast that a pressure wave cannot precede the disturbance.
- The conditions in the medium—temperature, density, bulk velocity—thus change almost instantaneously at the shock. The material which is hit by the shock receives no forewarning.



Shocks

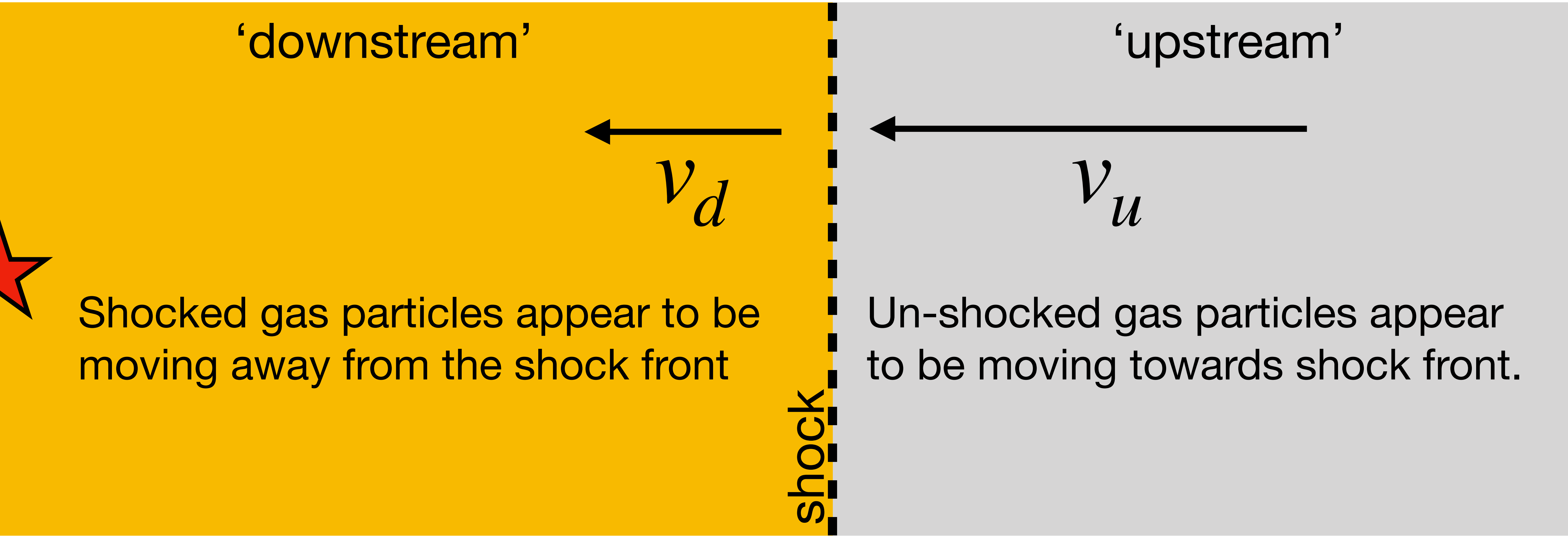
Derivation of strong shock 'jump conditions'



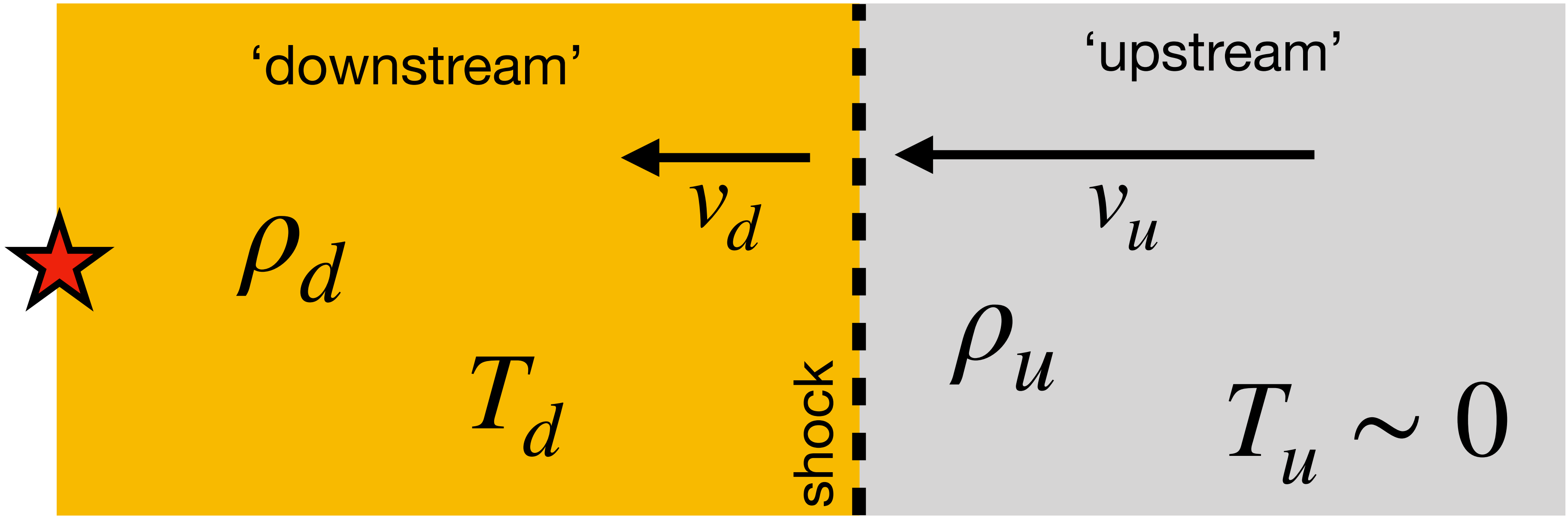
$$\rho_d > \rho_u$$

Shocks

Switch to rest frame of the shock



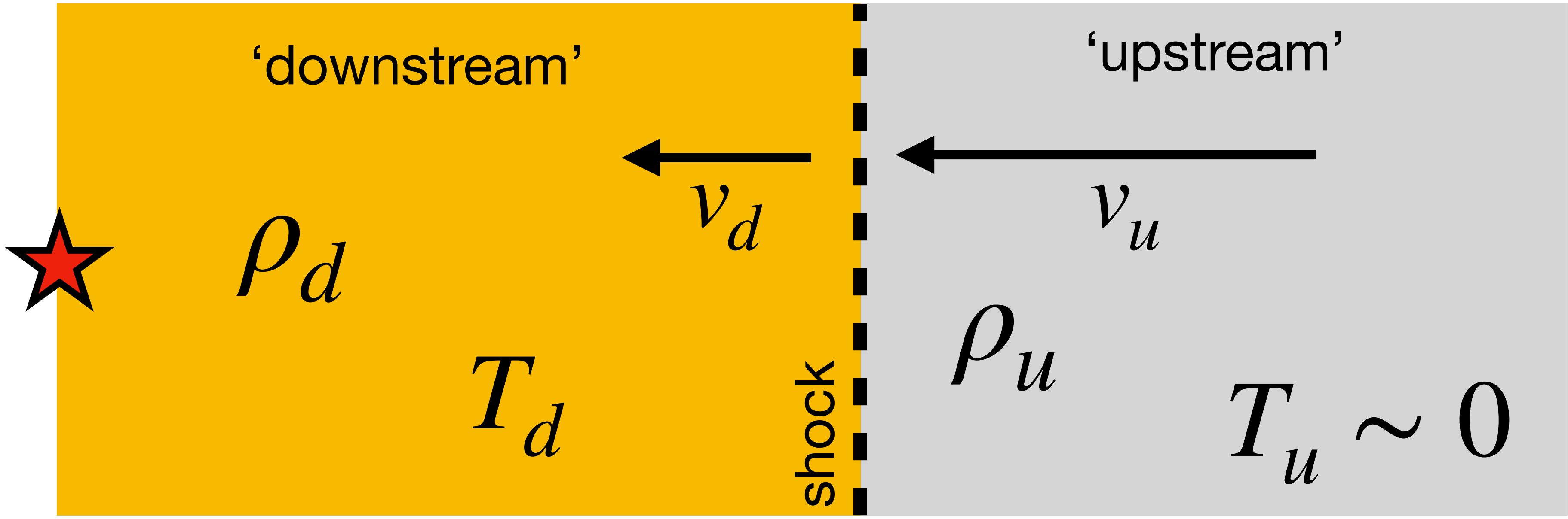
$$v_d < v_u$$



(1) Mass conservation:

$$\rho_d v_d = \rho_u v_u$$

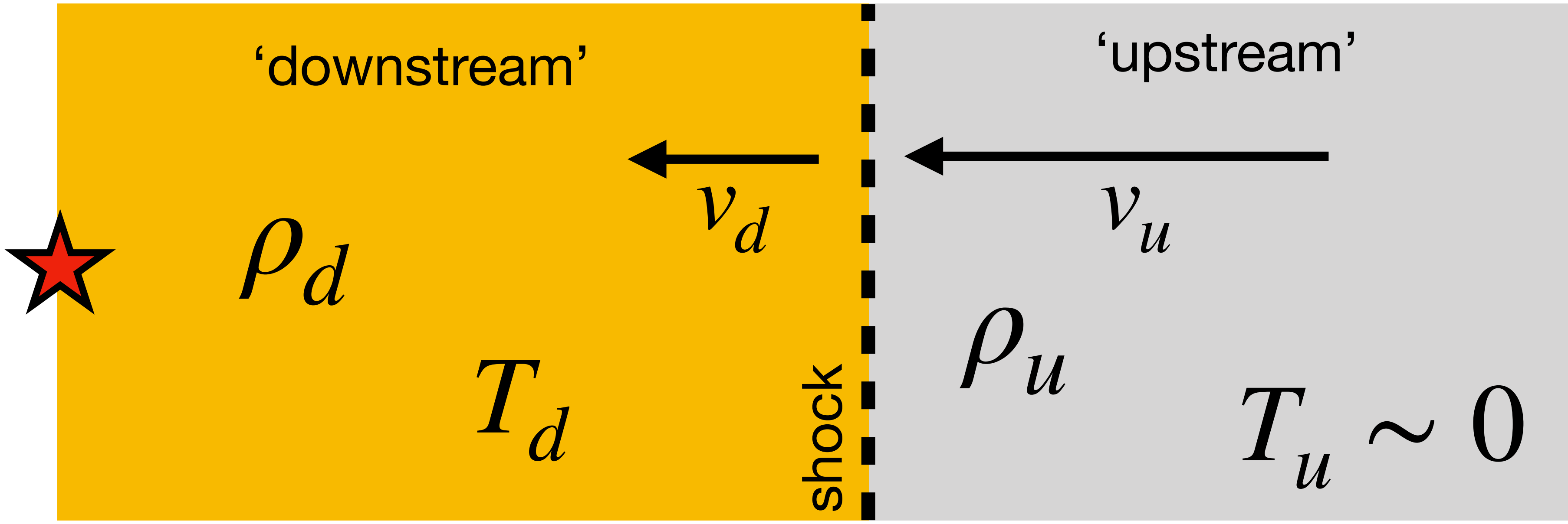
Mass per unit area flowing across shock front



(2) Momentum conservation:

Momentum per unit area flowing across shock front

$$P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$$

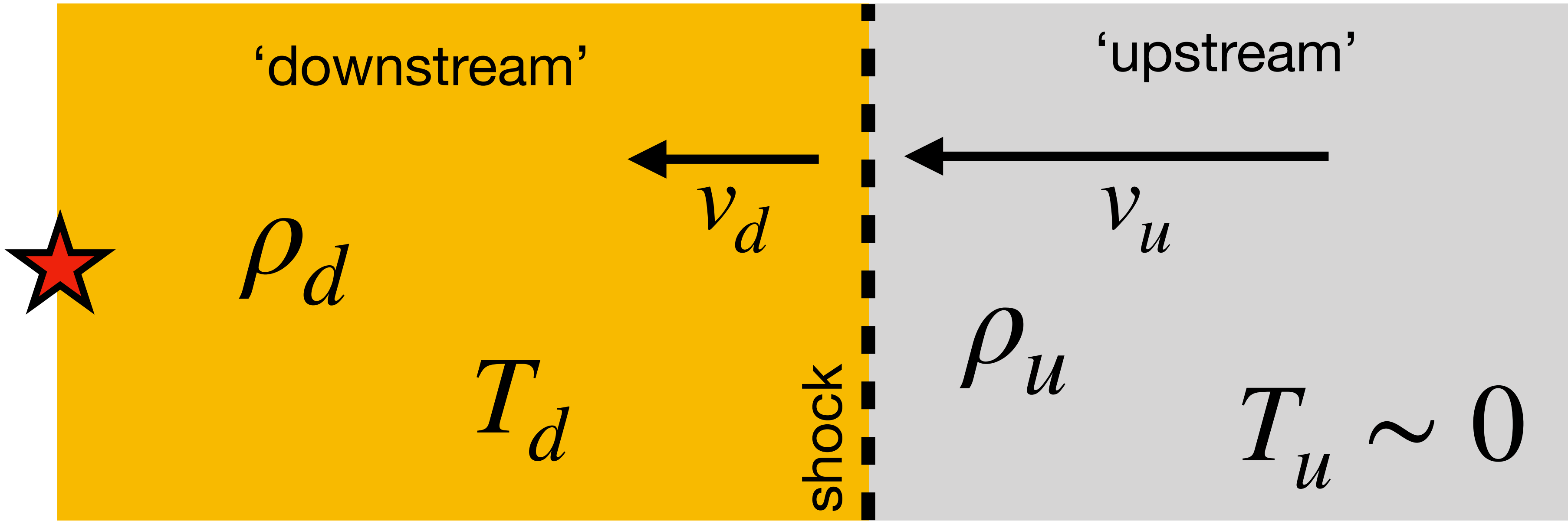


(2) Momentum conservation:

Momentum per unit area flowing across shock front

$$P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$$

Ram pressure (pressure from bulk motion)



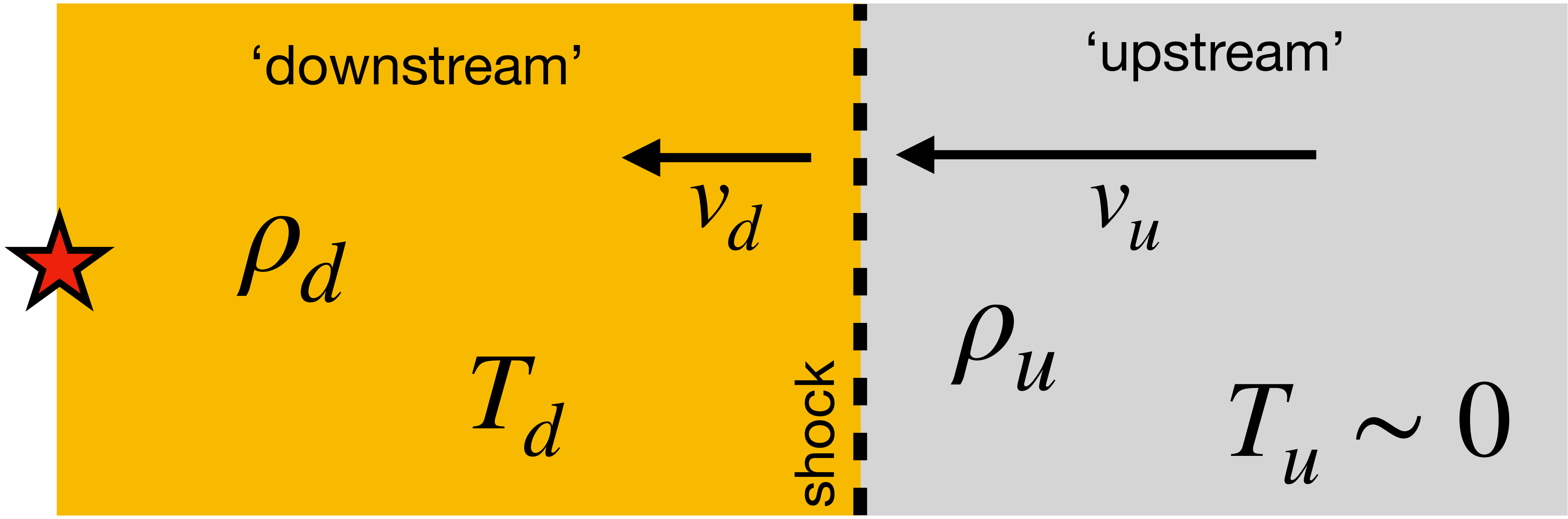
(2) Momentum conservation:

Momentum per unit area flowing across shock front

Gas pressure (pressure from thermal motions)

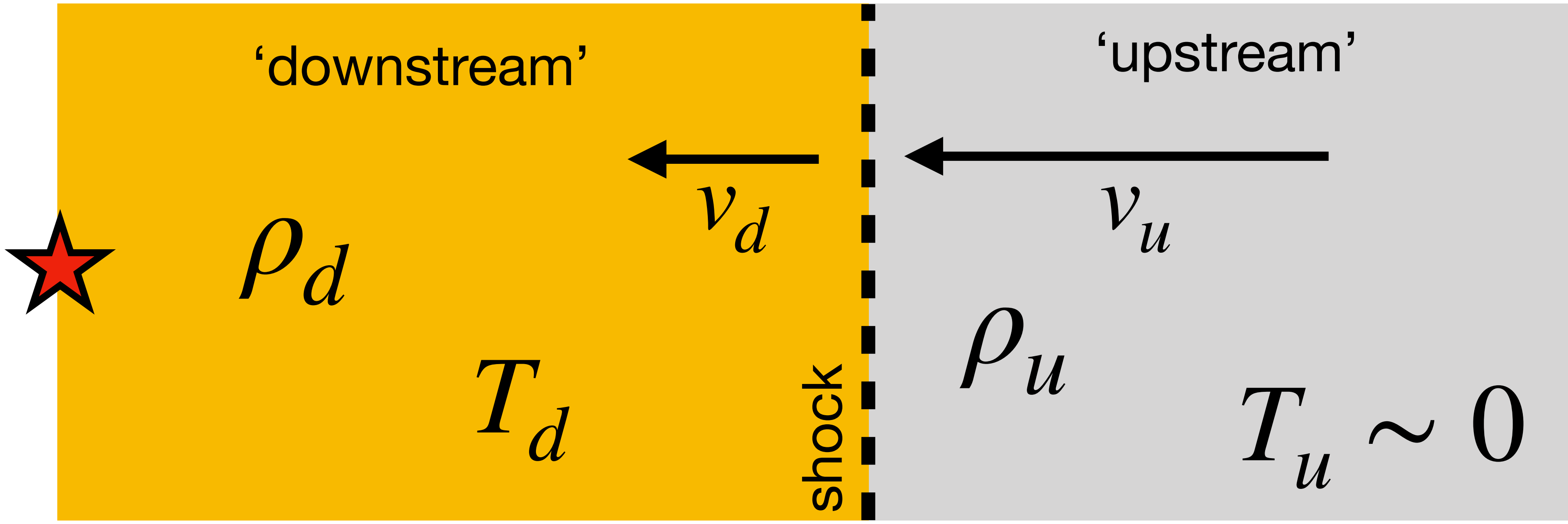
$$P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$$

Ram pressure (pressure from bulk motion)



(3) Energy conservation:

Energy per unit area flowing across shock front

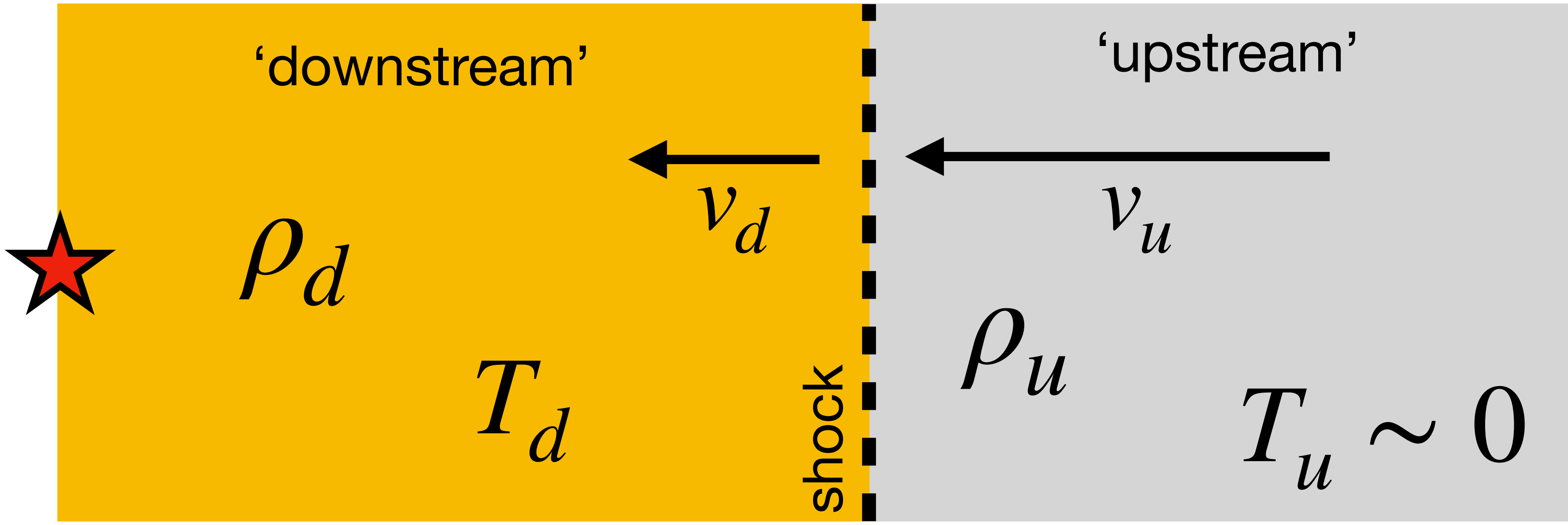


(3) Energy conservation:

Energy per unit area flowing across shock front

$$v_d \left[\frac{1}{2}\rho_d v_d^2 + \rho_d \epsilon_d\right] + P_d v_d = v_u \left[\frac{1}{2}\rho_u v_u^2 + \rho_u \epsilon_u\right] + P_u v_u$$

ε= internal energy per unit mass



(3) Energy conservation:

Energy per unit area flowing across shock front

$$\underbrace{v_d \left[\frac{1}{2} \rho_d v_d^2 + \rho_d \epsilon_d \right]}_{\text{energy / area / time}} + P_d v_d = v_u \left[\frac{1}{2} \rho_u v_u^2 + \rho_u \epsilon_u \right] + P_u v_u$$

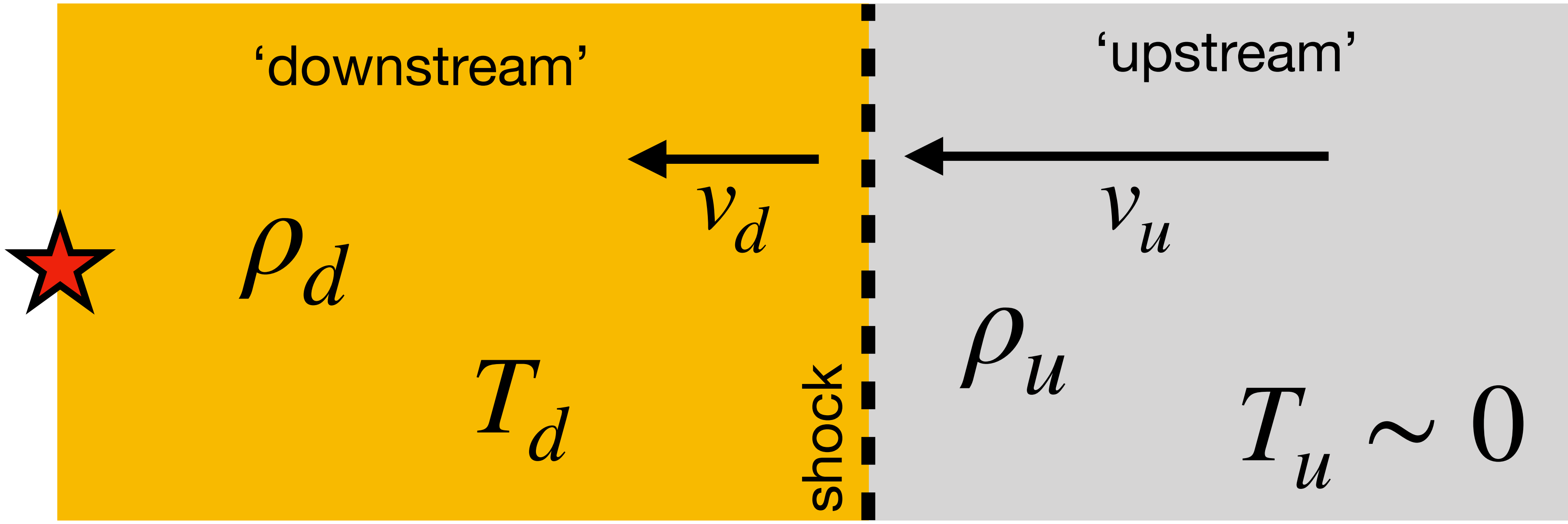
KE / volume

TE / volume

P dV work / area / time

energy / area / time

ε= internal energy per unit mass

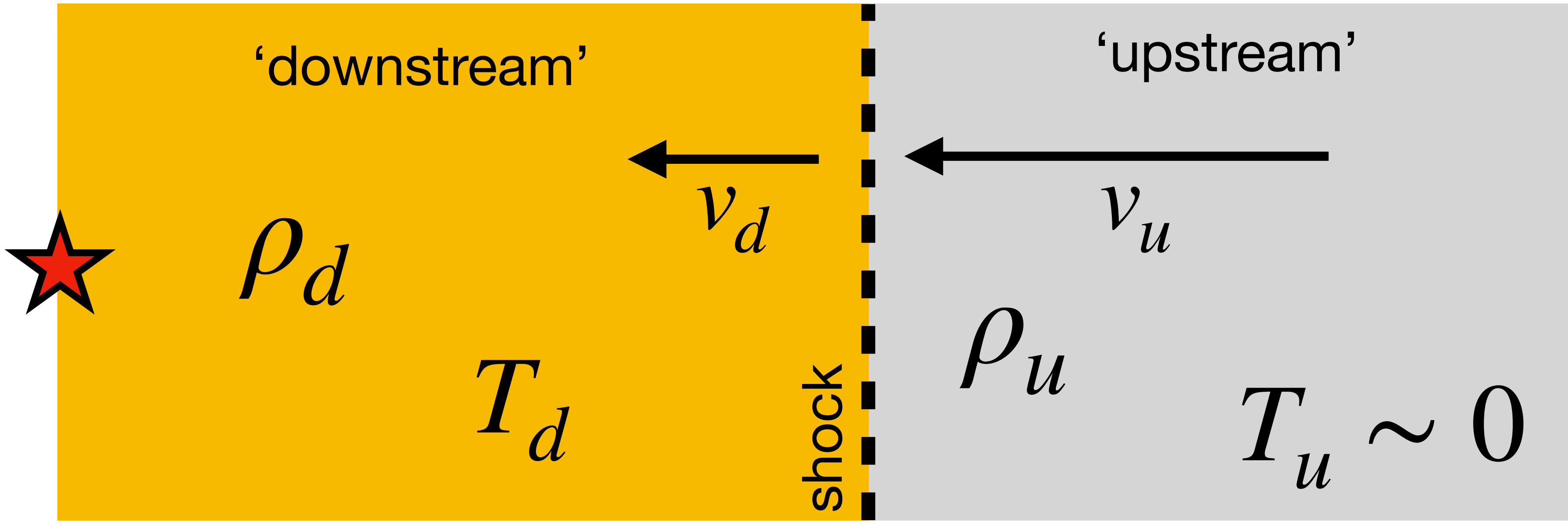


Rankine-Hugoniot jump conditions:

1) $\rho_d v_d = \rho_d v_u$

2) $P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$

3) $v_d \left[\frac{1}{2} \rho_d v_d^2 + \rho_d \epsilon_d \right] + P_d v_d = v_u \left[\frac{1}{2} \rho_u v_u^2 + \rho_u \epsilon_u \right] + P_u v_u$



Simplify (2):

$$P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$$

$$T_u \sim 0 \quad \Longrightarrow \quad P_u \sim 0 \quad \Longrightarrow$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

(3)

Simplify (2):

$$P_d + \rho_d v_d^2 = P_u + \rho_u v_u^2$$

$$T_u \sim 0 \implies P_u \sim 0 \implies$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

(3)

Simplify (3):

$$v_d \left[\frac{1}{2} \rho_d v_d^2 + \rho_d \epsilon_d \right] + P_d v_d = v_u \left[\frac{1}{2} \rho_u v_u^2 + \rho_u \epsilon_u \right] + P_u v_u$$

$$\rho_d v_d = \rho_u v_u \quad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \quad (2)$$

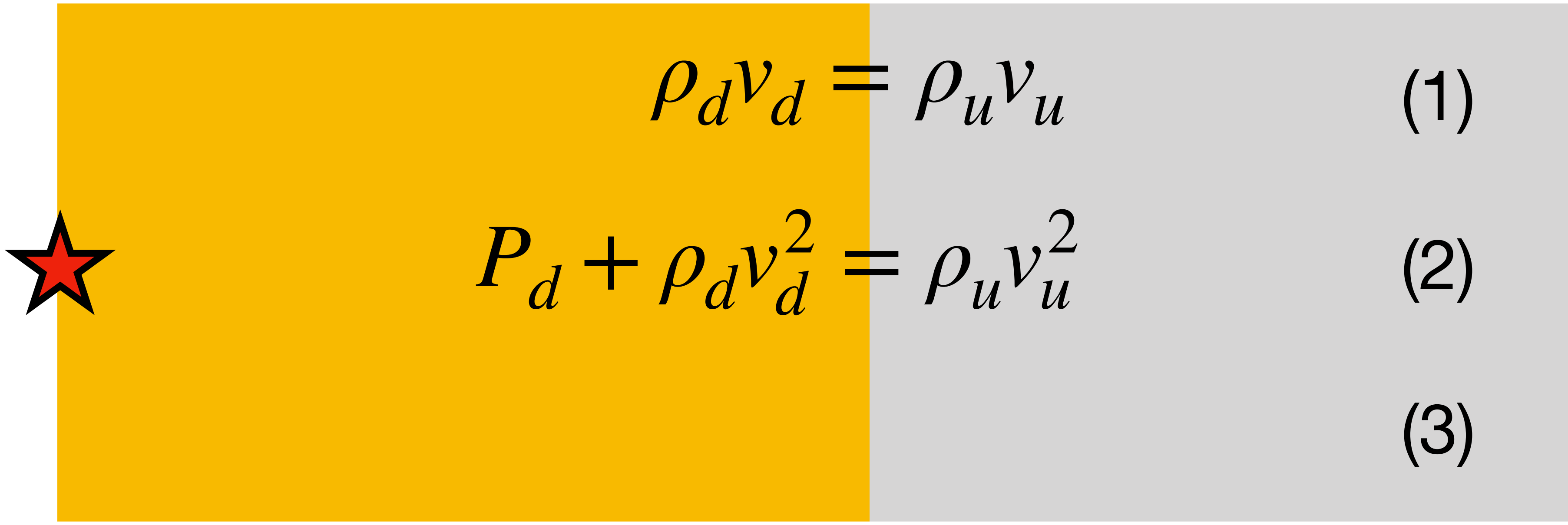
(3)

Simplify (3):

$$v_d \left[\frac{1}{2} \rho_d v_d^2 + \rho_d \epsilon_d \right] + P_d v_d = v_u \left[\frac{1}{2} \rho_u v_u^2 + \rho_u \epsilon_u \right] + P_u v_u$$

For ideal gas:

$$\epsilon = \frac{3}{2} \frac{kT}{\bar{m}} \qquad P = \frac{\rho}{\bar{m}} kT \qquad \therefore \qquad \rho\epsilon = \frac{3}{2} P$$



$$\rho_d v_d = \rho_u v_u \quad (1)$$

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(3)

Simplify (3):

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$$\Longrightarrow$$

$$v_d \left[\frac{1}{2} \rho_d v_d^2 + \frac{3}{2} P_d \right] + P_d v_d = v_u \frac{1}{2} \rho_u v_u^2$$

$$\rho_d v_d = \rho_u v_u \quad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \quad (2)$$

$$v_d \left[\frac{1}{2} \rho_d v_d^2 + \frac{3}{2} P_d \right] + P_d v_d = v_u \frac{1}{2} \rho_u v_u^2 \quad (3)$$

$$\rho_d v_d = \rho_u v_u \quad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \quad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2} P_d v_d = \frac{1}{2}\rho_u v_u^3 \quad (3)$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

$$(2) \Longrightarrow \qquad P_d = \rho_u v_u^2 - \rho_d v_d^2$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

(2) $\Longrightarrow \quad P_d = \rho_u v_u^2 - \rho_d v_d^2$

Sub into (3):

$$\Longrightarrow \quad \frac{1}{2}\rho_d v_d^3 - \frac{1}{2}\rho_u v_u^3 + \frac{5}{2}\rho_u v_u^2 v_d - \frac{5}{2}\rho_d v_d^3 = 0$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

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$$-\frac{1}{2}\rho_u v_u^3 - 2\rho_d v_d^3 + \frac{5}{2}\rho_u v_u^2 v_d = 0$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

(2) $\Longrightarrow$ $$P_d = \rho_u v_u^2 - \rho_d v_d^2$$

Sub into (3):

$$\Longrightarrow \quad \frac{1}{2}\rho_d v_d^3 - \frac{1}{2}\rho_u v_u^3 + \frac{5}{2}\rho_u v_u^2 v_d - \frac{5}{2}\rho_d v_d^3 = 0$$

$$-\frac{1}{2}\rho_u v_u^3 - 2\rho_d v_d^3 + \frac{5}{2}\rho_u v_u^2 v_d = 0$$

$\times -2$

$$\Longrightarrow \quad \rho_u v_u^3 + 4\rho_d v_d^3 - 5\rho_u v_u^2 v_d = 0$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

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Sub into (3):

$$\Longrightarrow \quad \frac{1}{2}\rho_d v_d^3 - \frac{1}{2}\rho_u v_u^3 + \frac{5}{2}\rho_u v_u^2 v_d - \frac{5}{2}\rho_d v_d^3 = 0$$

$$-\frac{1}{2}\rho_u v_u^3 - 2\rho_d v_d^3 + \frac{5}{2}\rho_u v_u^2 v_d = 0$$

$\times - 2$

$$\Longrightarrow \quad \rho_u v_u^3 + 4\rho_d v_d^3 - 5\rho_u v_u^2 v_d = 0$$

Sub in (1):

$$\Longrightarrow \quad \rho_u v_u^3 + 4\frac{\rho_u^3}{\rho_d^2} v_u^3 - 5\frac{\rho_u^2}{\rho_d} v_u^3 = 0$$

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

(2) $\Longrightarrow$ $$P_d = \rho_u v_u^2 - \rho_d v_d^2$$

Sub into (3):

$$\Longrightarrow \quad \frac{1}{2}\rho_d v_d^3 - \frac{1}{2}\rho_u v_u^3 + \frac{5}{2}\rho_u v_u^2 v_d - \frac{5}{2}\rho_d v_d^3 = 0$$

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$\times -2$

$$\Longrightarrow \quad \rho_u v_u^3 + 4\rho_d v_d^3 - 5\rho_u v_u^2 v_d = 0$$

Sub in (1):

$$\Longrightarrow \quad \rho_u \cancel{v_u^3} + 4\frac{\rho_u^3}{\rho_d^2}\cancel{v_u^3} - 5\frac{\rho_u^2}{\rho_d}\cancel{v_u^3} = 0$$

$$\rho_d v_d = \rho_u v_u \tag{1}$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \tag{2}$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \tag{3}$$

$$\rho_u \cancel{v_u^3} + 4\frac{\rho_u^3}{\rho_d^2}\cancel{v_u^3} - 5\frac{\rho_u^2}{\rho_d}\cancel{v_u^3} = 0$$

$$\rho_d v_d = \rho_u v_u \quad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \quad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \quad (3)$$

$$\rho_u \cancel{v_u^3} + 4\frac{\rho_u^3}{\rho_d^2}\cancel{v_u^3} - 5\frac{\rho_u^2}{\rho_d}\cancel{v_u^3} = 0$$

$$\times \frac{\rho_d^2}{\rho_u^3} \implies \left(\frac{\rho_d}{\rho_u}\right)^2 + 4 - 5\frac{\rho_d}{\rho_u} = 0$$

$$\rho_d v_d = \rho_u v_u \tag{1}$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \tag{2}$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2}P_d v_d = \frac{1}{2}\rho_u v_u^3 \tag{3}$$

$$\rho_u \cancel{v_u^3} + 4\frac{\rho_u^3}{\rho_d^2}\cancel{v_u^3} - 5\frac{\rho_u^2}{\rho_d}\cancel{v_u^3} = 0$$

$$\times \frac{\rho_d^2}{\rho_u^3} \quad \Longrightarrow \quad \left(\frac{\rho_d}{\rho_u}\right)^2 + 4 - 5\frac{\rho_d}{\rho_u} = 0$$

$$\left(\frac{\rho_d}{\rho_u} - 1\right)\left(\frac{\rho_d}{\rho_u} - 4\right) = 0$$

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Trivial: $v_d = v_u; \quad \rho_d = \rho_u$

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Trivial: $v_d = v_u; \quad \rho_d = \rho_u$

Strong shock!

$$\rho_d v_d = \rho_u v_u \qquad (1)$$

$$P_d + \rho_d v_d^2 = \rho_u v_u^2 \qquad (2)$$

$$\frac{1}{2}\rho_d v_d^3 + \frac{5}{2} P_d v_d = \frac{1}{2}\rho_u v_u^3 \qquad (3)$$

Strong shock jump conditions:

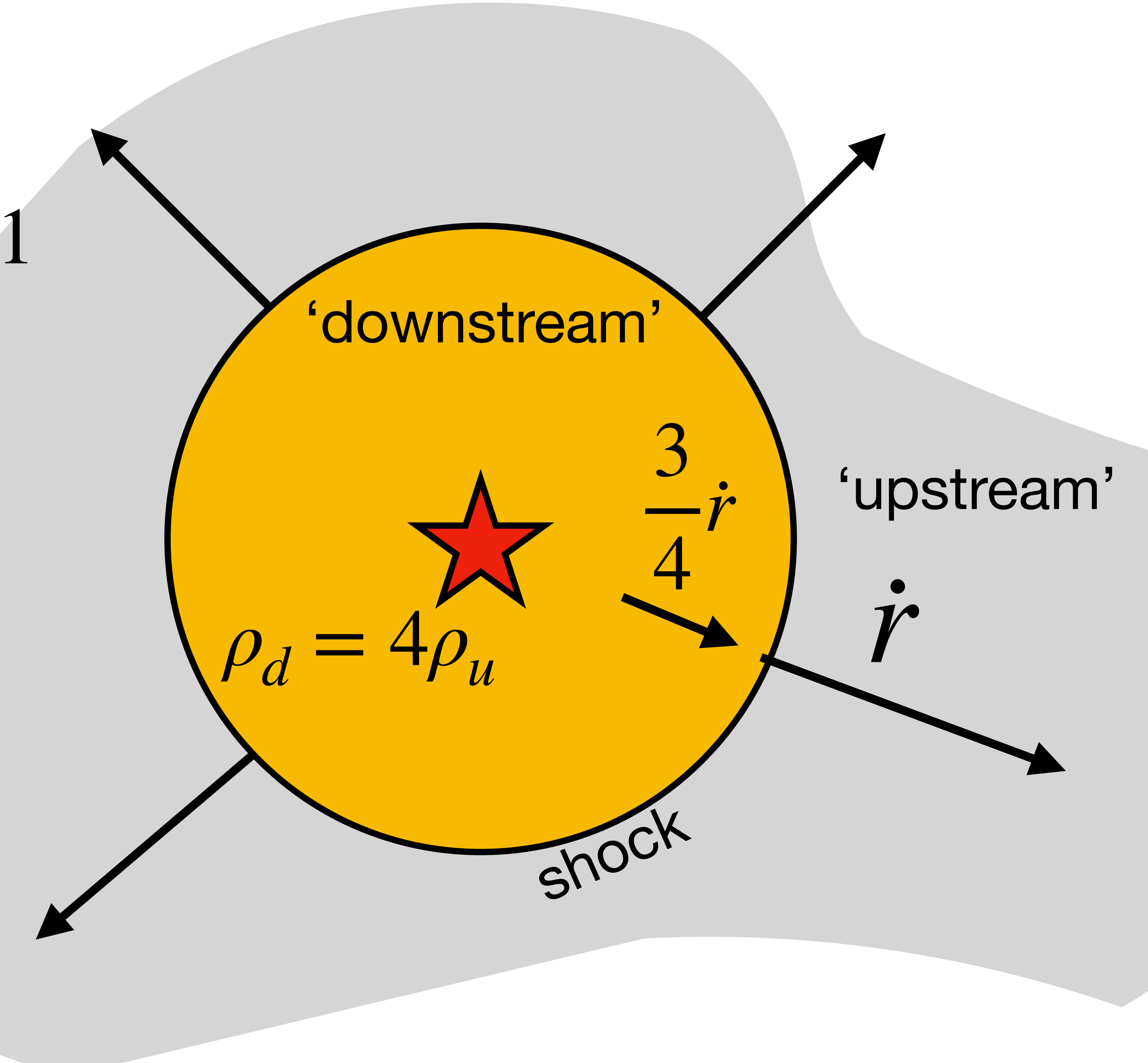
$$\boxed{\frac{\rho_d}{\rho_u} = 4} \qquad \boxed{\frac{v_u}{v_d} = 4}$$

Shocks

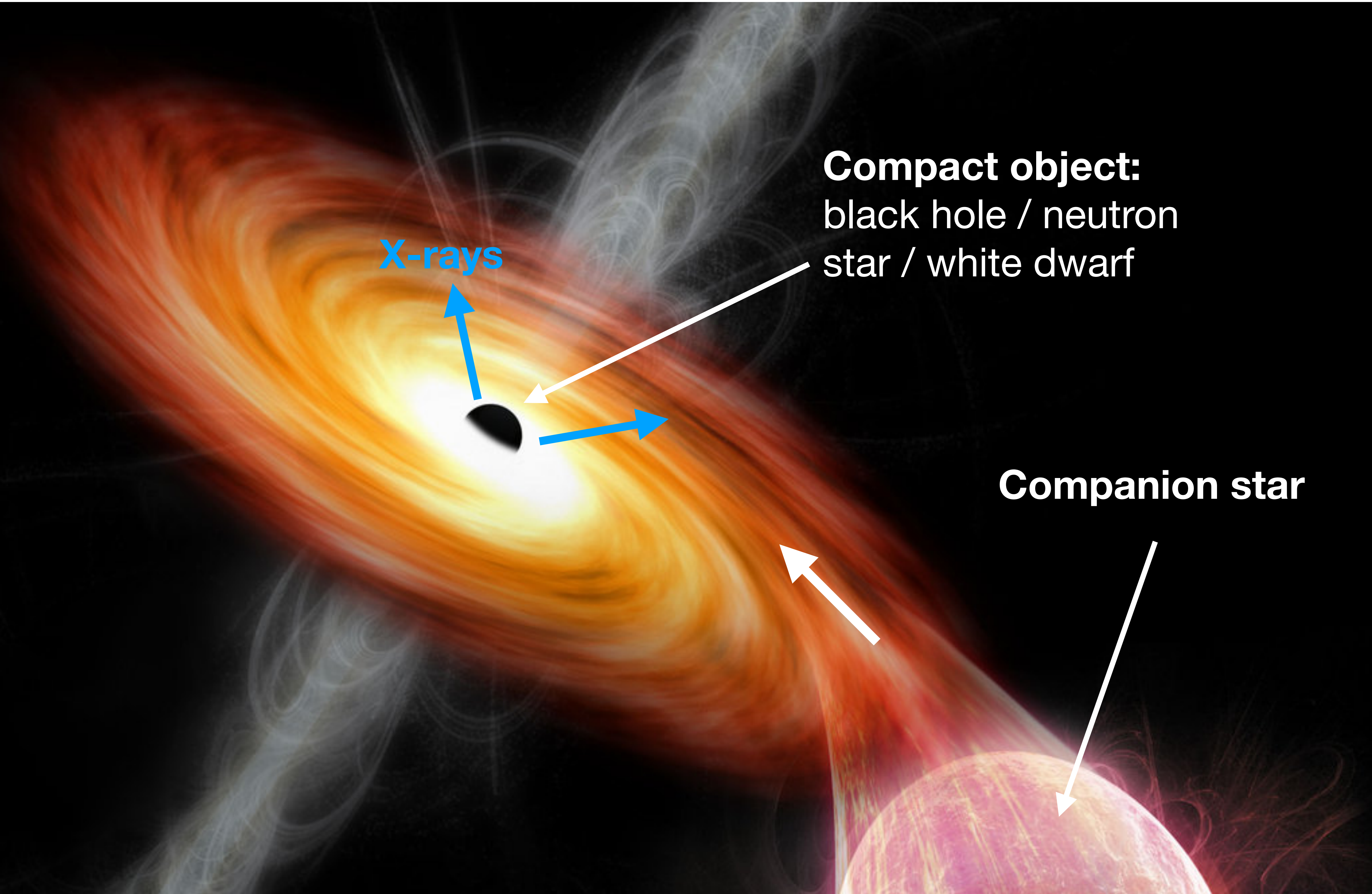
Back in the rest frame of the ISM

Assumptions:

- Ideal gas, T.E./m=(3/2)kT
- Mach number: $\mathscr{M} \equiv v/c_s \gg 1$
- $T_u \sim 0$
- Ignored viscosity (only important within mean free path from shock front)



Compact object accretion



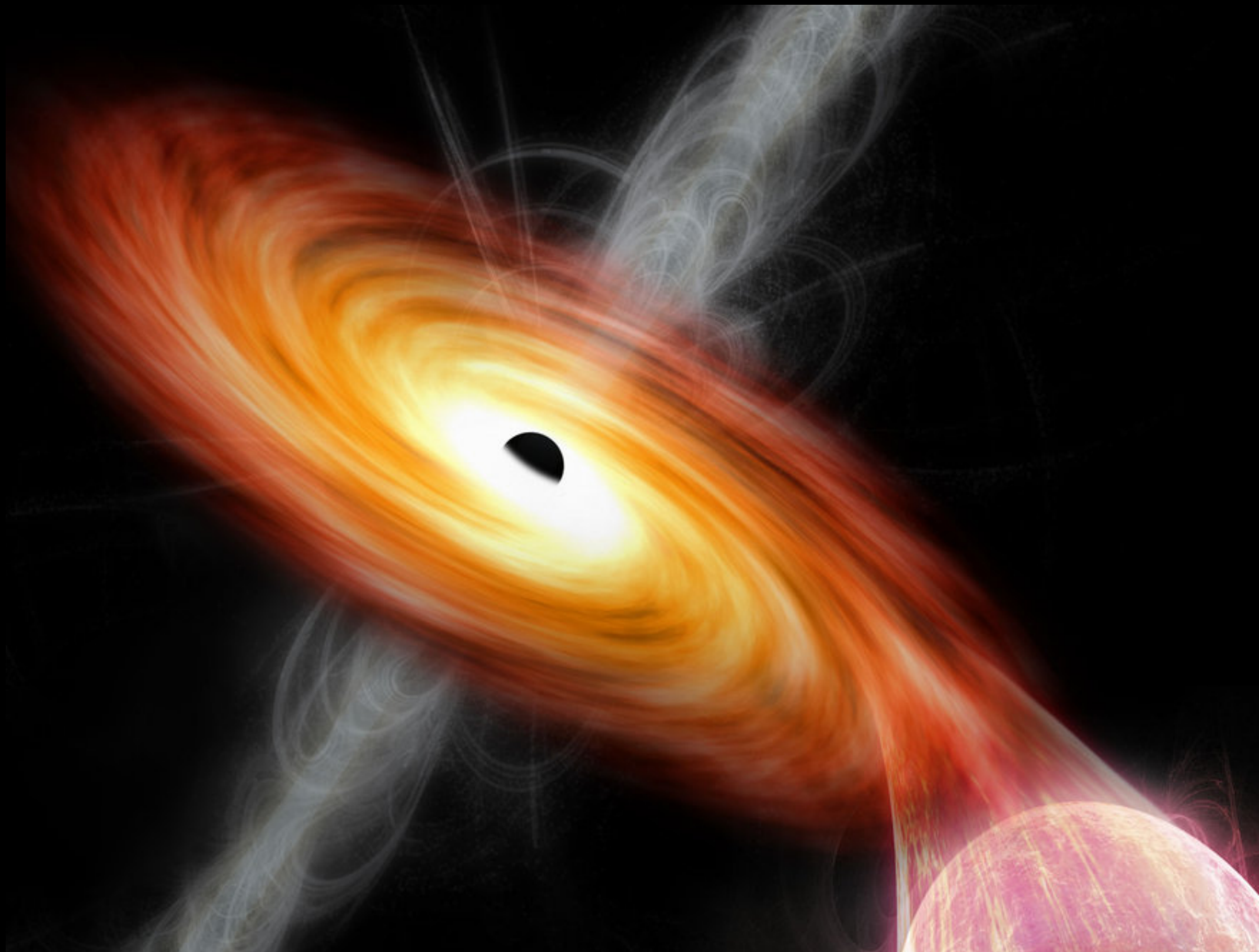
Compact object accretion

- Compact object = black hole or neutron star: system called an X-ray binary
- Compact object = white dwarf: system called cataclysmic variable or dwarf nova (historic)
- White dwarf systems: WD always observed to be more massive than companion
- High mass X-ray binaries (HMXBs):

$$M_{\mathrm{companion}} > M_{\mathrm{co}}$$

- Low mass X-ray binaries (LMXBs):

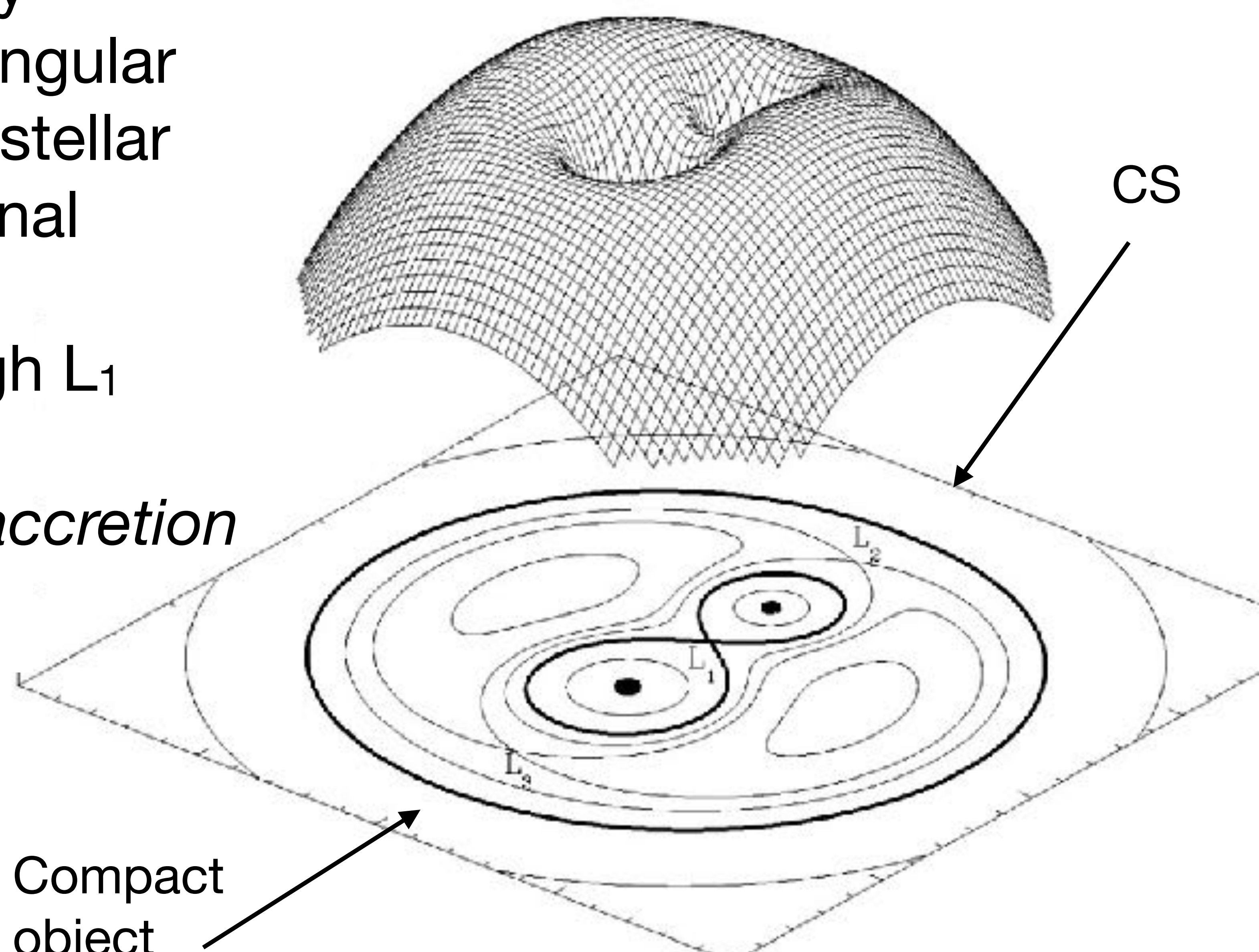
$$M_{\mathrm{companion}} < M_{\mathrm{co}}$$



Compact object accretion

LMXBs: Roche-Lobe Overflow

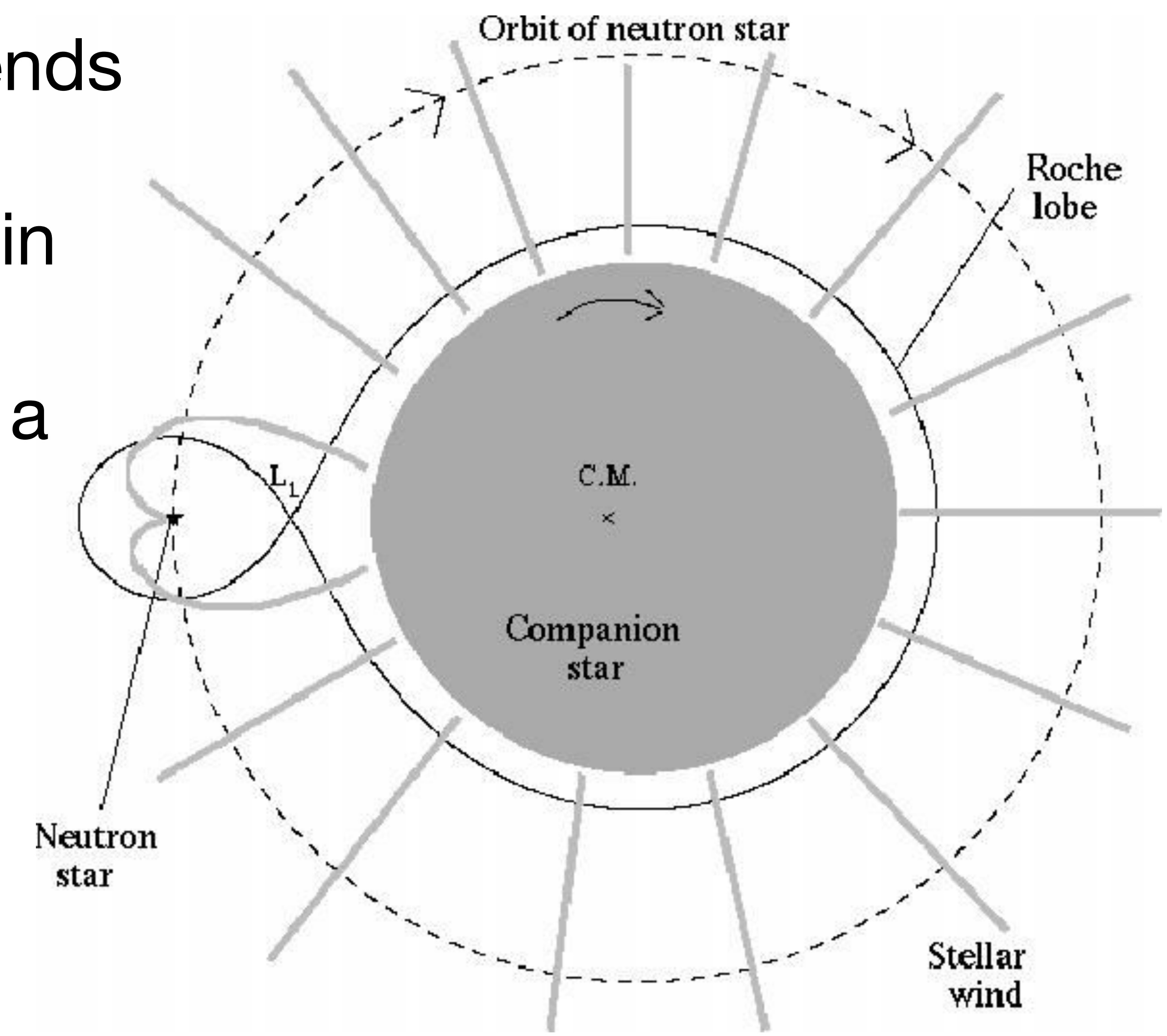
- *Roche potential*: companion star (CS) occupies equipotential surface.
- CS can fill its *Roche Lobe* if it swells during its evolution, *or* binary separation reduces due to angular momentum loss due to e.g. stellar wind mass loss or gravitational waves.
- Then material passes through L_1 (inner Lagrange point).
- In-falling material forms an *accretion disc*



Compact object accretion

HMXBs: Stellar Wind Capture

- $M \gtrsim 15\ M_{\odot}$ stars can have a strong stellar wind.
- Wind can be captured by the compact object.
- Accretion luminosity therefore depends on mass outflow rate of wind.
- Can also get Roche-Lobe overflow in HMXBs, but less common
- Intermediate case: Cygnus X-1 has a focused wind

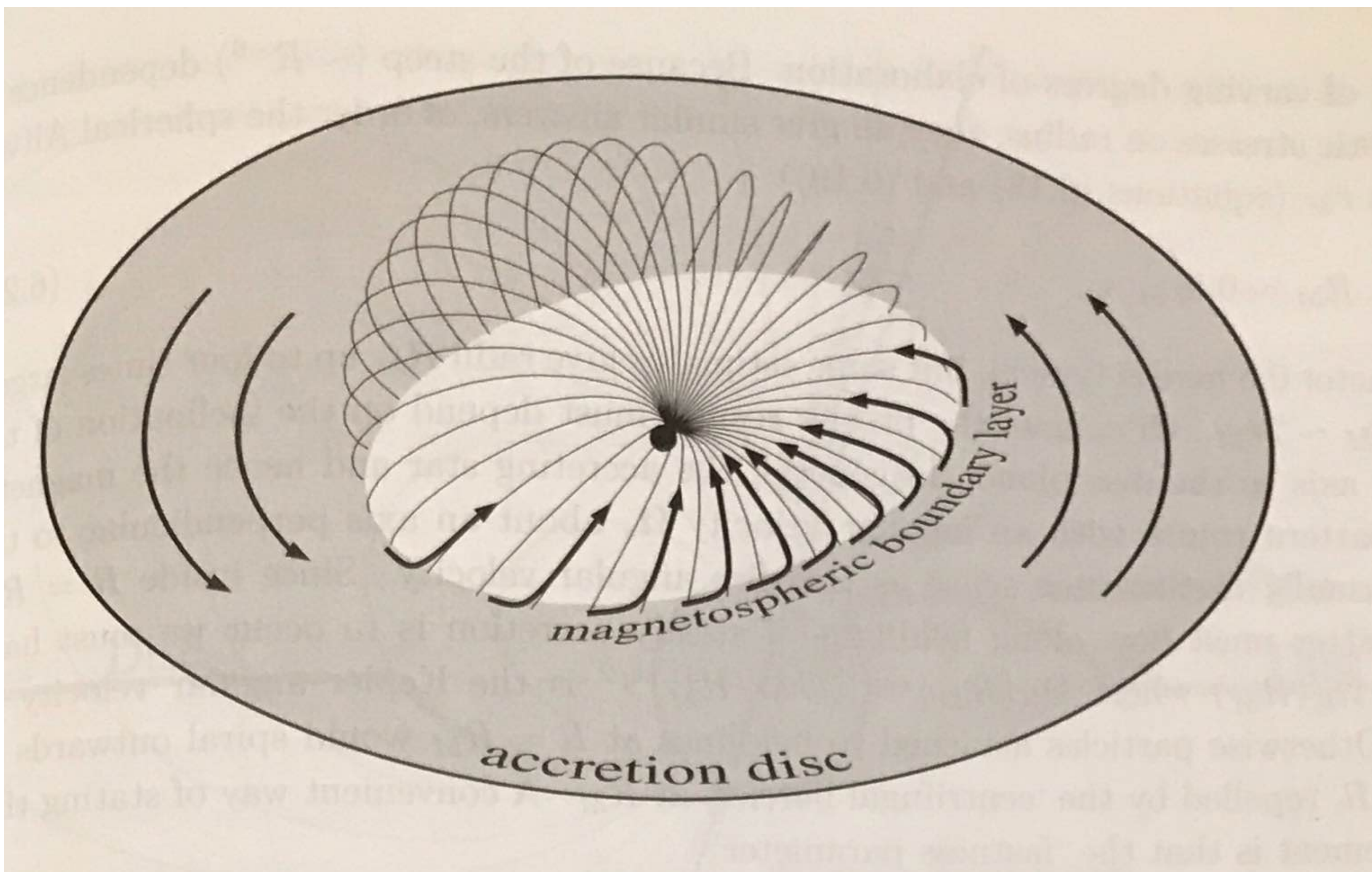


Compact object accretion

Magnetic fields

- B-field of NS / WD can interrupt disc and channel material directly to magnetic poles.

CV (white dwarf) / X-ray pulsar (neutron star)

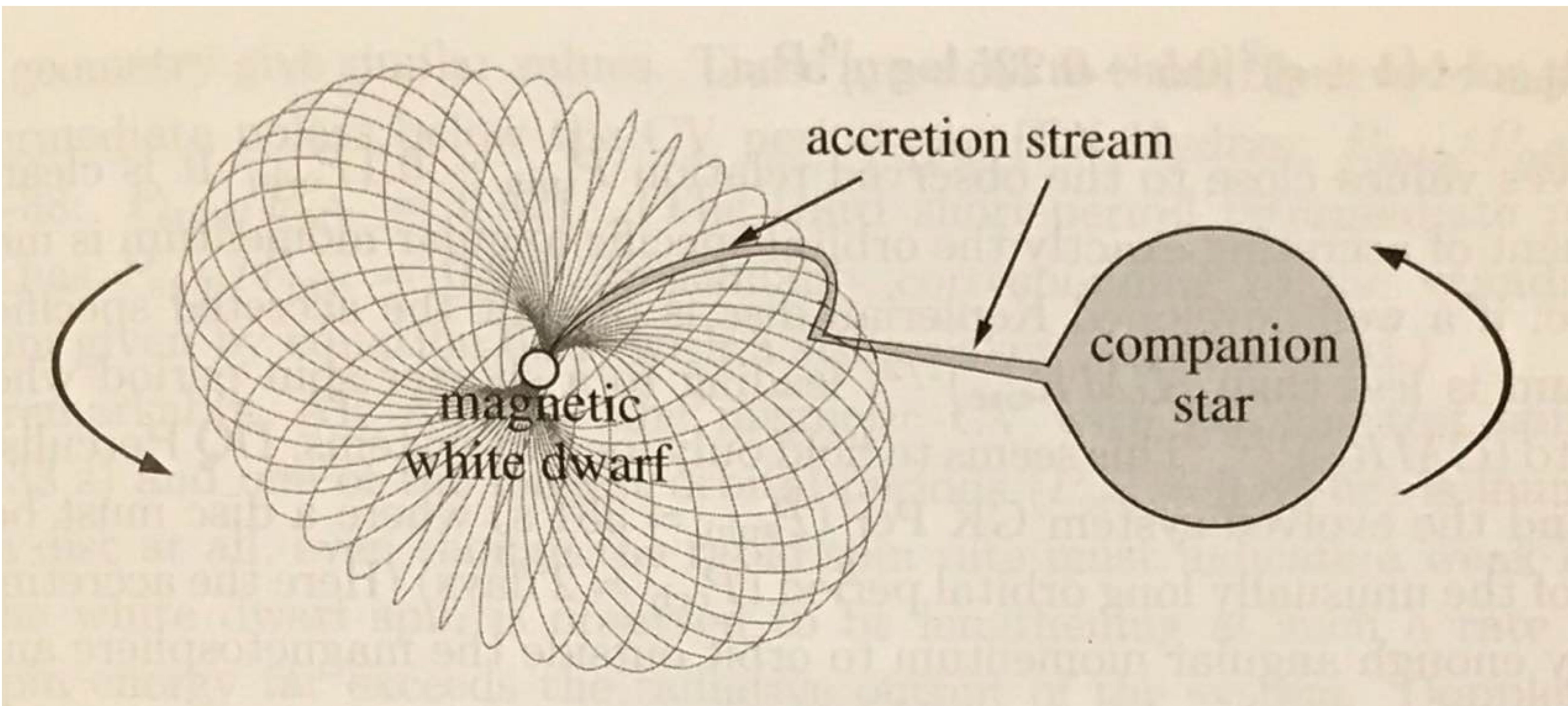


Compact object accretion

Magnetic fields

- B-field of NS / WD can interrupt disc and channel material directly to magnetic poles.
- For strongest field WDs, there can be no disc at all.

Polar



Compact object accretion

Magnetic fields

- Gravitational free fall in accretion column
- Shock as material is halted
- Homework problem: calculate T_d (hot enough to emit hard X-rays)